INSDAG YEARBOOK 2020-2021





INSTITUTE FOR STEEL DEVELOPMENT AND GROWTH (INSDAG)

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Steel is the backbone of all industries and the basic ingredient for growth and development of a country. Traditionally, the fortunes of the steel industry have been linked to the economic cycle of the country. Per capita consumption of steel speaks volumes about the relative position of the country on the development frontier. In India the per capita consumption of steel stands low compared to developed and developing countries. Moreover, steel is completely recyclable and environment friendly. Hence, a large potential exists in furthering the usage of steel in various segments of industry. Institute of Steel Development and Growth (INSDAG), a non-profit making, member based organization established by Ministry of Steel and the major steel producers of the country. The Institute primarily works towards the development of advanced design methodologies & technical marketing by expanding applications of steel in different segments of industry, upgrading skills & know-how, creating awareness amongst potential users and communicating the benefits of steel. Our founding members are SAIL, Tata Steel Ltd., RINL, JSW Steel Ltd., and Arcelor Mittal Nippon Steel India Limited (AM / NS) apart from Ministry of Steel. INSDAG has got very good networking among the member organisations/professionals for exchange of ideas. The Institute is registered as a "Society" under Societies Registration Act of West Bengal.

INSDAG

Director General looks after the daily affairs of the Institute and Executive Council provides guidance and direction. Two other functional committees namely the Working Group and Project Review Committee provide administrative and technical guidance respectively. The Institute has defined its mission, role, and functions and has evolved its short, medium and long term Activity Plans. The Institute primarily works towards the development of technology in steel usage and the market for the steel fraternity. Some of its roles are:

- Creating awareness amongst potential users on affordability of steel.
- > Bringing out technical publication on steel applications.
- > Providing technical advisory services on materials, construction practices etc.
- > Upgrading the skills of work force by refresher courses / training programmers.
- > Communicating the benefits of steel through life cycle cost studies.
- > Providing requisite thrust to increase steel consumption in rural areas.
- > Assisting in the development of ancillary industries for creating new market.

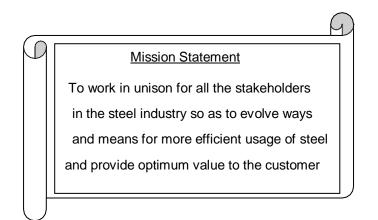
INSDAG Year Book 2020-2021

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PREFACE

The primary drivers of steel consumption in the country would be massive infrastructure as well as the progress of a number of s teel intensive s tructures like machinery & equipment, consumer durables and automobiles.

INSDAG Yearbook 2020 - 2021 contains the technical articles from experts in steel industry. The document contains article like Economy is Hallmark of Parallel Flange Sections – A Boon to the Indian Steel Construction Industry by Mr. Pydi Lakshma na Rao, Steel Concrete Composite Columns by Mr. Arijit Guha, Corrosion in Industrial Steel Structures and Mitigation by Mr. Pratip Bhattacharya; Mr. Manos Kumar De, High Strength Structural Steels by Mr. Asim Kum ar Sam anta, Efficient Construction with Steel Weld Mesh F abric by Dr Jayanta Kumar Saha, Innovative Usage of Steel Hollow Sections in Steelbased Construction by Mr. Ravi Kumar, A Journey into the World of Corrosion by Ms. Sohini Mitra, Transitioning to High Strength Steel for Structural Applications by Mr. Tamilselvan; Mr. Sahil Aggarwal; Dr PC Ashwin Kumar .

We believe that the range and scope covered by the technical papers in the yearbook covering the high strength steels, new steel materials like welded wire mesh, parallel flange sections, composite construction, corrosion protection of steel structures and innovative use of steel hollow sections will definitely create interest in steel fraternity and increased use of steel intensive structures.

INSDAG Year Book 2020-2021

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ECONOMY IS THE HALLMARK OF PARALLEL FLANGE SECTIONS - A BOON TO INDIAN STEEL CONSTRUCTION INDUSTRY

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General Manager (C&S) Institute for Steel Development & Growth

INTRDUCTION

A structural engineer's responsibility is to design the structural members of buildings, bridges, dams, offshore platforms etc, with maximum efficiency and minimum cost satisfying the strength and stiffness requirements. Selecting the suitable structural arrangement, design methodology and choosing the right structural sections of required strength can accomplish the economy.

In dia n s t a n dard medium section s a re available in one size only for each bea m dept h. However, in case of parallel fla nge bea m s (in view of t he Universal Rolling Technology), more n um ber of bea m s h aving t he sa me bea m dept h b u t with varying flange and web thick ness, flange widt h s and weight per unit lengt h (Fig. 1) will be available giving more flexibility to t he designers & economy to the owner.

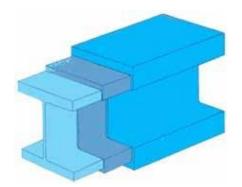


Fig.1: Various Shapes with Equal Chamber Size

With the setting up of a major Rail & Universal Beam Rolling Mill at their Raigar h works in Chh attisgar h, J SPL (J in dal Steel & Power Limited) is the first Com pany in the In dia n market to prod u ce much-awaited tailor made hot rolled parallel flange bea ms and colum ns of wide range up to 900 mm dept h. These beams and columns are well accepted by consultants, designers and fabricators because of their substantial cost benefit over convention ally available tapered beams or built up sections. Steel Au thority of In dia Limited (SAIL) is producing NPB, WPB sections confirming to IS: 808-2021 (For merly IS: 12778) and HE sections confirming to DIN 1025. These sections are available from NPB 100x 55x 8.1 to NPB 750x 270x 202.5, WPB 160x 160x 23.8 to WPB 450x 300x 171.12 from their Universal rolling mills at ISP, Burnpur and DSP, Durgapur.

These section s a re available in different grades as per IS 2062-2011 and also able to prod u ce copper bearing s tr u ct ural's to increase corrosion resistance. These grades are rolled as per customer's specifications.

Parallel Fla nge Section s from SAIL a re also available in t he following foreign specification s such as ASTM-A-36, JIS-G-3101-SS400, BS-4360 (Grades 40A, 43A, 43B, M 43C, 50B, 50C), EN-10025 (Grades S-275 JO, JR, S-335 JO, JR), DIN-17100 (Grades ST 37.2/44.2) as mentioned in their website (www.sail.co.in).

Parallel flange sections produced by SAIL and JSPL are available in different grades with yield strength of 250 to 450 MPa. These sections can be welded easily. Parallel flange I-Sections to be used as beams of nominal size range s from 180x90 mm to 900x300 mm and column sections from 150x150 mm to 400x400 mm are being produced and are made available in domestic market by JSPL leading to significant economy in steel construction.

With the availability of large number of beams with different statical properties having the same beam depth besides having the advantage of parallel flange over taper flange will give the designers, architects and construction agencies great flexibility in choosing the right sections depending on applications. Also these sections have better sectional properties (section modulus, radius of gyration) compared to conventional I - Beams which are produced now in India. The load carrying capacity of parallel flange sections is higher under direct compression compared to that of similar I-Sections available today. Also connections to the flanges are simpler since no tapered washers etc. are required.

In view of above it is highly recommen ded to h ave t he efficient parallel fla nge sections in construction industry to bring down the overall cost of the s tr u ct u res. Almost all t he co u n tries (Ger m a ny, J apa n, USA etc.) u se t hese efficient parallel fla nge section s a n d h ave t heir own n a tion al st a n dards for t he same.

The present IS: 808-2021 dealing with parallel flange section covers sections u pto 900 mm bea m dept h. This I n dia n Sta n dard incorporates a wide of r a nge sections with proper grouping upto 900 mm dept h.

MAJOR ADVANTAGES OF PARALLEL FLANGE BEAMS

Possibility of broad range of statical properties having the same depth of beams permitting selection of the most optimum flange width and thickness and web thickness Mu ch better section al properties s u ch as section mod ulu s a n d radiu s of gyration. Parallel fla nge bea m s exhibit much higher load carrying capacity under direct compression

Parallel flange I sections used as beams offer substantial savings in cost

Connection s to the flanges are simpler since no was hers are required (Fig.2)

Butt Welding of plates at the edge of flanges is easier



Fig.2: Easy Connections Using Parallel Flange Sections

AVAILABILITY

Parallel flange beams are available in three categories

- 1. Narrow flange beams (NPB)
- 2. Wide flange beams (WPB)
- 3. Bearing pile section s (PBP)

Narrow and wide flange beams can be supplied in any of the three subcategories

Light weight
 Standard
 Weight 3. Heavy
 weight

MATERIAL GRADES

These sections can be supplied in material grades conforming to IS: 2062-2011. Grades E 250, E 300, E 350, E 400, E 450 are manufactured by JSPL.

SECTIONAL SPECIFICATIONS

Parallel Flange Sections shall be made as per British, German, American or any other international specifications in addition to the Indian specification.

At present parallel flange sections are available from SAIL upto a maximum depth of 900 mm and width 300 mm with varying flange and web thickness which are available from their state-of the art Universal Rolling Mill. Sections will confirm to the tolerance limits of IS: 1852 and they can also be produced to any other international standard.

APPLICATION OF PARALLEL FLANGE SECTIONS

Parallel flange sections are invariably used in developed countries in almost all civil engineering structures like bridges, railway stations, car parks, buildings, stadiums, shopping complexes etc., due to their excellent statical properties and flexibility in choosing right section. Connections are simpler in case of parallel flange sections. This will helps to reduce the overall structure cost. Parallel Flange Sections particularly UC sections are suitable for columns. Large column free spans are possible using parallel flange sections with high grade steel. Number of columns can be reduced by 50% in Multi level Car Parks as per the study report (INS/PUB/019) prepared by INSDAG.

SAVINGS IN MATERIAL AND MONEY

Parallel flange section s and bearing pile section s can be used as beams and columns in steel structures, without going for fabricated or compound sections. Rolled section is always preferable to avoid extra fabrication cost.

The weight of s teel bea m / colum n req uired will be less in case of parallel fla nge section s compared to conventional ISMB sections. The advantages of parallel fla nge section s with respect to ISMB section s are shown in Fig. 3, Fig. 4, Fig. 5, Fig. 6, Fig. 7 and Fig. 8.

Fig.3 shows that the saving in material by using PFS in comparison to ISMB.

Fig.4 shows that saving in material under compression Load. For example, to carry 500 kN by a member, use of either NPB 200x165x35.7 @ 35.7 kg/m or UC 152X152 @ 37 kg/m is enough compared to ISMB 400 @ 61.5 Kg/m.

Fig.6 shows that the range of bending capacity of parallel flange sections is much higher than that of ISMB.

Fig.7 shows that bending capacity of a parallel flange beam is always higher than that of ISMB for almost equal weight.

This is evident from the graphs indicating the axial compression capacities of parallel flange sections are higher compared to ISMB sections of similar weight.

Similarly the section al weight of parallel flange section s is lower compared to ISMB sections for carrying same axial compression loads. Another big

adva n t age is t h a t t hese parallel fla nge section s a re now available in differen t grades conforming to IS: 2062 - 2011 which will definitely reduce the steel structure cost considerably.

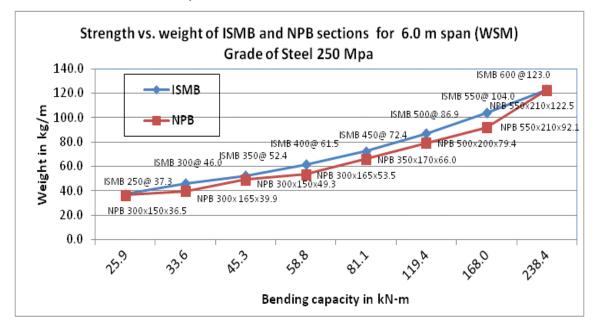


Fig.3: Weight of Steel Beam for Different Bending Moment Values

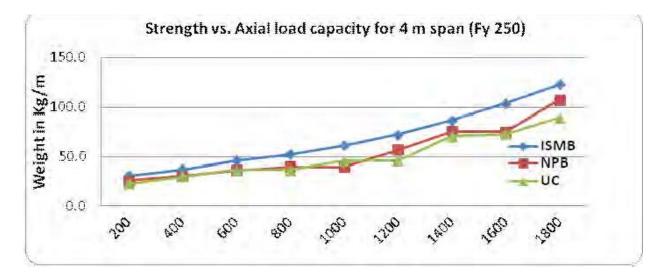


Fig.4: Weight of Steel Column for Different Axial Loads

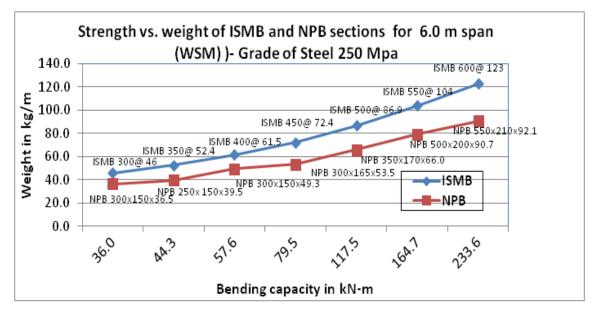


Fig 5: Strength vs. Weight of ISMB and NPB Sections

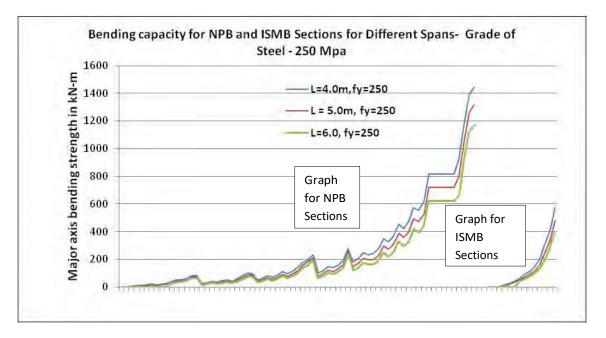


Fig. 6: Bending Capacity for NPB and ISMB Sections for Different Spans

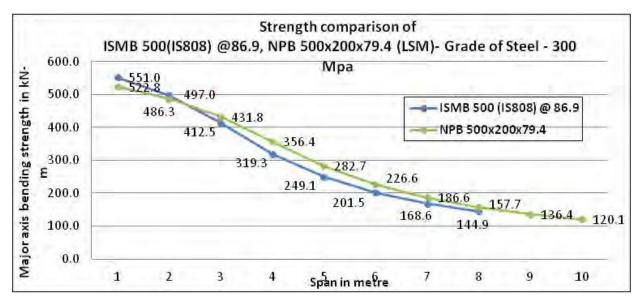


Fig. 7: Strength Comparison of ISMB 500, NPB 500x200x79.4 (LSM)

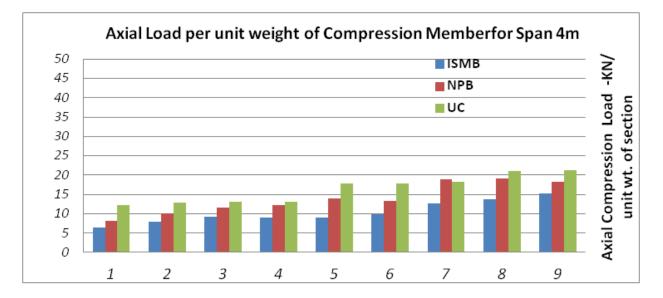


Fig 8: Axial Load per Unit Weight of Compression Member for Span 4m



Fig. 9: Car Park with PF Sections

The use of parallel flange sections is very useful where column-free long span a re req uired. Multi-level Car Parks (Fig.9) is one such structure where more column free area is required for easy manoeuvring of vehicles.

CONCLUSIONS

Efficient parallel flange sections up to 900 mm depth are now available from Steel Authority of India and Jindal Steel & Power, JSPL.

The use of parallel flange sections reduces the use of 3-plated sections thereby reducing the fabrication work and increase the speed of construction.

Facilitates the long column free structures

Weight saving will be around 10-25% in case of bending members & 20-40% in case of axial compression member . The use of Parallel Flange Sections results in overall saving in material and cost of steel structures.

The savings are much higher if high strengt h parallel flange section s are used.

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STEEL-CONCRETE COMPOSITE COLUMNS

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ABSTRACT

Some of the steel-based construction in the country so far has seen composite construction where the beams have been designed as composite with the slab supported by it on top. The earlier relevant code IS: 11384 – 1985 gave the Limit States Design for these beams. No stipulations or theory or guidelines were available to design composite elements like Columns. Also, the code did not cover composite slab. Hence, wherever required, most of the structures and its composite elements were designed with the help of foreign codes, mostly British or Eurocodes

The present draft code for composite construction IS: 11384 - 2022, gives guidance for design of all types of composite elements in structure, be it slab, beam or column. This article is aimed at giving a very brief outline and guidance about the utility of composite columns, its types and basic design procedure.

INTRODUCTION

Steel-concrete composite construction is an advanced technology which combines the compressive strength of Concrete with the tensile strength of steel to evolve an effective and economic structural system. Over the years this specialized field of construction has become more and more popular in the western world and has developed into a multifaceted design and construction technique. Steel-concrete composite construction over the last few years is getting highly popularized in the In dia n scen ario, but is still limited to commercial structures like multiplexes, some in du strial structures, a few multi-storied constructions and road bridges. In this construction, structural steel work is typically used together with concrete; for example, s teel beams with concrete floor slabs to attain composite action. This applies to buildings, road bridges, where concrete decks are normally preferred. Steel and concrete have almost the same thermal expansion apart from an ideal combination of strengths. Hence, these essentially different materials are completely compatible and complementary to each other.

Most of the steel-concrete com posite construction till date has seen the use of composite beam along with steel columns and RCC slab. These is due to the fact that the earlier relevant design code IS: 11384 - 1985 dealt with only the design of com posite beams. No stip ulation s or theory or guidelines were available to design composite elements like columns which carry axial loads

as well as bi-axial bending moments. Also, the code did not cover composite slab wherein a thin concrete slab with minimum reinforcements acts together with the supporting steel profiled sheet, with or without embossments. The steel sheet acts as shuttering and provides for tensile strength of the slab against bending moment. The present revised code IS: 11384 -2022, gives guidance for design of all types of composite elements in structure, be it slab or beam or column.

COMPOSITE COLUMNS AND TYPE

Columns are elements which carry all the loads from slabs, beams, etc., and transfer them to the foundation, and are thus the most vital elements in a structure. The present code has laid down detailed principles and guidelines to design composite columns which will enable a designer to utilize the strengt hof both the materials in the most judicious way to make the most rational design of a steel-based structure.

A steel-concrete com posite colum n is a com pression mem ber, com prising eit her a concrete encased hot-rolled/plated steel section or a concrete filled t u b ular section of hot-rolled / plated s teel a n d is generally u sed as a loadbearing mem ber in a composite framed structure. Typical cross-sections of com posite colum n s wit h fully a n d partially concrete encased s teel section s a re illu s tra ted in Fig. 1. Fig. 2 shows three typical cross-section s of concrete filled t u b ular section s. It may be noted, t h at there is no requirement to provide addition al reinforcing s teel for com posite concrete filled t u b ular section s, except for requirements of fire resistance where appropriate.

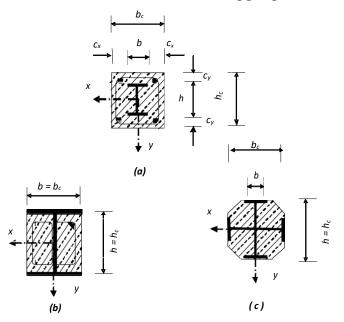


Fig.1: Typical Cross - Sections of Fully and Partially Concrete Encased Columns

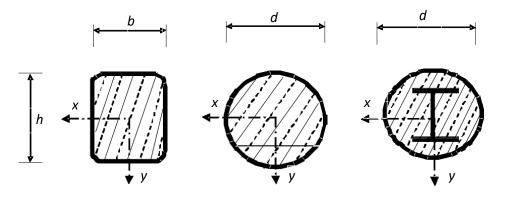


Fig.2: Typical Cross-Sections of Concrete Filled Tubular Sections

The initial development of composite columns was based on the need for providing effective fire protection for steel in buildings. It was common to encase the steel section within concrete. The weak concretes provided, resulted in very less enh ancement in the overall strengt hof the section. Increase in strengt h and stiffness due to concrete encasement was ignored in the past, although increase in buckling resistance of the overall column was recognized. By the early part of the 1960's decade, studies showed that concrete encasement increases the load resistance of the steel columns. In addition to it, substantial economy in construction costs could be achieved by using better quality of concrete and ensuring composite action with steel by mutual interaction through chemical bond and friction or by using mechanical shear connectors in certain circumstances.

Provision of supplementary reinforcement in the concrete encasement prevents excessive spalling of concrete both under nor mal load and fire conditions. Concrete encased steel composite columns have become preferred structural form for earthquake resistant structures across the world.

ADVANTAGES

For a column in composite construction, initially the bare steel sections support all the construction loads, including the weight of structure during construction. Concrete is later cast around the steel section, or filled in side the tubular sections. The lighter weight and higher strengt hof steel per mit the use of s maller and lighter foundations. The subsequent addition of concrete to complete the composite column element enables the building frame to easily limit the sway and lateral deflections. With the use of composite columns along with composite decking and composite beams it is possible to erect high rise structures in an extremely efficient manner and in a much faster pace requiring lesser time than conventional RCC or non-composite steel structures. The advantages of composite columns are:

Higher strength for a given cross section al dimension.

- Higher s tiffness, leading to red u ced slen der ness and higher buckling resistance.
- Good fire resistance in the case of concrete encased columns. However, for concrete filled tubes active or passive fire resistance measures need to be taken just like for pure steel columns

Better protection to corrosion in encased columns.

Significant economic advant ages over either pure structural steel or reinforced concrete alternatives, more so for concrete filled steel tubes.

Iden tical cross section s with different load and moment resistances can be produced by varying steel thickness, the concrete strength and reinforcement. This allows the outer dimensions of a column to be held constant over a number of floors in a building, thus simplifying the construction and architectural detailing.

Erection of high rise building in an extremely efficient manner.

For mwork is not required for concrete filled tubular sections.

DESIGN OF COMPOSITE COLUMNS

Like all structural elements, a composite column must also be designed for the Ultim ate Limit State. For structural adequacy, the internal forces and moments resulting from the most unfavorable load combinations hould not exceed the design resistance of the composite cross-sections. While local buckling of the steel sections may be eliminated due to bonding with surrounding concrete, the reduction in the compression resistance of the composite columndue to overall buckling should definitely be considered toget her with the effects of residual stresses and initial imperfections. Moreover, the second order effects in slender columns as well as the effect of creep and shrin kage of concrete under long term loading must be considered, if they are significant. The reduction in flex ur al stiffness due to cracking of the concrete in the tension area should also be considered.

At present, for design of composite columns, or for that matter any composite element, the relevant BIS code, IS: 11384 - 2022, may be referred for general steel construction. However, the relevant codes for steel bridges, IRC: 22 – 2015, may also be followed for all composite columns, till the new BIS code comes out. The method of design suggested in these codes, incorporates the latest research on composite construction. Isolated symmetric columns having uniform cross sections in braced/non-sway and moment resisting frames may be designed by the simplified design method described in these codes. This method also

adopts the E u ropea n b u ckling c u rves for s teel colum n s as the basis of colum n design. The sim plified met hod is for mulated for pris m a tic com posite colum n s with dou bly symmetrical cross-section s. The calc ulation s of variou s design para meters a re covered and the checks for s truct u r al adeq u acy of a com posite colum n u n der applied loads a re men tioned these codes. The ultim a te safety of the colum n com ponen t is achieved by a ttaining the following bou n dary conditions as per the two codes mentioned above.

$$P \le P_d$$
 (i)

$$\frac{M_x}{\mu_{dx}M_{dx}} + \frac{M_y}{\mu_{dy}M_{dy}} \le 1$$
(ii)

$$\frac{M_x}{\mu_{dx}M_{dx}} \le \alpha_{mx} \tag{iii}$$

$$\frac{M_y}{\mu_{dy}M_{dy}} \le \alpha_{my} \tag{iv}$$

where,

P = Factored Applied Axial Load

- P_d = Permissible Axial Force considering lateral Buckling.
- M = Factored Design Moment in the two orthogonal axes of the colum n
- M_d = Design Ben ding Resista nce of the section about the ben ding axis, evaluated as in section

 μ_{dx} and μ_{dy} = Moment resistance reduction factors in x and y directions, respectively

 a_{mx} and a_{my} = reduction coefficient based on steel yield strength in x and y directions;

= 0.9 for $f_y \leq 400$ MPa

 $= 0.8 \text{ for } f_y > 400 \text{ MPa}$

FIRE RESISTANCE

D u e to t he t her m al m ass of concrete, com posite colum n s always possess a higher fire resistance than corresponding steel colum ns. Com posite colum ns a re u s u ally designed in the normal or 'cool' state and then checked under fire condition s. Addition al reinforcement is sometimes required to achieve the target fire resistance. Some general rules on the structural performance of composite columns in fire are summarised as follows:

The fire resistance of composite columns with fully concrete encased steel sections may be treated in the same way as reinforced concrete

colum ns. The steel is in sulated by an appropriate concrete cover and light reinforcement is also required in order to maintain the integrity of the concrete cover. In such cases, two-hour fire resistance can usually be achieved with the minimum concrete cover of 40 mm.

For composite columns with partially concrete encased steel sections, the structural performance of the columns is very different in fire, as the flanges of the steel sections are exposed and less concrete acts as a 'heat shield'. In general, a fire resistance of up to one hour can be achieved if the strength of concrete is neglected in normal design. Additional reinforcement is often required to achieve more than one-hour fire resistance.

For concrete filled tubular sections subjected to fire, the steel sections are exposed to direct heating while the concrete core beh aves as 'heat sink'. In general, sufficient redistribution of stress occurs between the hot steel sections and the relatively cool concrete core, so that a fire resistance of one hour can usually be achieved.

For longer periods of fire resistance, additional reinforcement may be provided. Steel fiberreinforcement is also effective in improving the fire resistance of a concrete filled column. It is also a practice in India to wrap the column with ferrocement to increase the fire rating. With the advent of Fire-Resistant Steel, the issue of fire resistance has become more easily solved up to 600° C.

CONCLUSION

Steel is very s trong material, especially in ten sion. It s higher s trengt h to weight ratio puts this material in a superior position compared to other materials of construction. However, on account of many discouraging factors s u ch as corrosion and lack of resistance in compression etc. does not allow it to be obvious choice of users.

Concrete is very s trong in com pression (though it has no ten sile s trengt h) and easy availability in s m all q u an tity m akes it pop ular con s tr u ction m a terial. It lack of tensile strength is compensated by giving steel reinforcement within the concrete members of structure.

Developed countries have taken advantages of both the materials by adopting the concept of composite construction technology for structure. They have developed the standards for it long back. EN 1994 (popularly known as Eurocode 4: Design of composite steel and concrete structures) is one such international code developed in Europe more than 40 years back.

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CORROSION IN INDUSTRIAL STEEL STRUCTURES AND MITIGATION

Pratip Bhattacharya

Manos Kumar De

Depart men t of Civil E ngineering Tata Consulting Engineers Limited

INTRODUCTION

The subject of corrosion is associated with many aspects of various branches of chemistry, metallurgy, metal physics, and bacteriology. Scien tific studies have revealed that few billions of dollars of nation al wealt h are lost annually due to corrosion of metals of daily use. Reasons of many premature failures of metallic structures and components are due to undeterred corrosion of metal parts. With the advancement of material science, the causes and control of many aspects of corrosion have been established but even then, the corrosion science is still under investigation and will continue to be so due to the inherent complexity. The article presents a brief ou tline only on at mosp heric corrosion of iron and steel, the most common engineering metal and the sim plest form of protection by use of selective painting/organic coatings.

DEFINITION OF CORROSION

Precise definition of the process of corrosion is difficult and controversial. L. L. S heer h as given a logical definition of corrosion as a com bin a tion of processes in which a metal or alloy used as construction material is transfor med from metallic to com bined state during interaction with the elements of the environment. Metals are generally reactive and except for noble metals they tend to exist in nature as com bined stable forms in oxides, sulphates, carbonates etc. Metal extraction processes are designed to recover the metal in pure form from these com pound forms of ores, but upon expos ure to environment the metals tend to revert to stable com pound forms. Metals are useful in pure forms and such conversion during the use is undesirable. Corrosion is defined as the 'undesirable deterioration' of a metal. It is an interaction of the metal with the environment which adversely affects the useful properties of the metal.

It may be noted that corrosion is not detriment al in all sit u ation s. The oxidized metal coats the surface and prevents further corrosion by hindering the access of metal with oxygen.

BASIC PRINCIPLES OF CORROSION

Corrosion has been defined as the process of transformation of metal to more stable compound form. Metal atom changes to ionic form by losing electron s in n a tural environment where they are absorbed by other atom s. The rusting of iron takes place in presence of simulta neo us presence of water and oxygen in the environment. The chemical reactions are given here.

$$H_2 O \rightleftharpoons H^+ + OH^- \tag{1}$$

Fe (metal) \rightleftharpoons Fe⁺⁺ + 2e (2)

 $2H^+ + 2e \rightarrow 2H \text{ atom s}$ (3)

2H atom s
$$\rightarrow$$
 H₂ gas (prevalent in acidic medium) (3a)

 $2H + \frac{1}{2} O_2 \rightarrow H_2 O \tag{3b}$

Fe⁺⁺ + 2 (OH)⁻
$$\rightarrow$$
 Fe(OH)₂ (in soluble rust) (4)

Further oxidation of Fe(OH)₂ in presence of air or dissolved oxygen proceeds:

4
$$Fe(OH)_2 + O_2 \rightarrow 2Fe_2O_3.H_2O + H_2O$$
, (stable rust) (5)

Rusting of iron under wet condition will not proceed unless reaction 3b proceeds and for which presence of oxygen is essential.

Corrosion can therefore be represented through the simple chemical reaction.

$$aA + bB = cC + dD \tag{6}$$

Where,

A = Metal, B = Non-metal reactants playing as oxidants C & D = the products of reaction.

The non-metallic reactant "B" represents the "Environment", although in a complex environment, the major constituents may play only subsidiary role in the reaction. Though atmosphere contains 78% nitrogen, its effect on a t mosp heric corrosion of iron and steel is negligible com pared to oxygen, carbon dioxide, s ulp h ur dioxide, and salt particles (in coastal environmen t). However, nitrogen plays critical role in specific cases like reaction of titanium with air at high temperatures.

TYPES OF CORROSION

Gaivanic Corrosion

As illustrated earlier corrosion involves flow of electrons from the metal to moist ure in at mosp here, ground, salt solution or from one part of metal surface to anot her at different galvanic potential. A corrosion cell is forme d with the metal forming the anode end (positive potential) and the surrounding medium forms the cathode (negative potential).

Galvanic corrosion occurring between dissimilar metals is another common principle of corrosion. When such dissimilar metals are immersed in electrolyte (acidic or salt solution) and connected by wire, current flow con tin u es till the anode metal en d dissolves in the electrolyte. Table 1 list s galva nic series of metals that can form such electrode pairs. This principle is used in design of cathodic protection of steel for underground installations or in seabed. A metal with higher galvanic potential like magnesium or zinc is bon ded to the steel surface. This metal forms the sacrificial anode and protects the steel by forming a coating on its surface¹.

Corroded End, Active, Anodic, Less Noble	Protected End, Passive, Cathodic, Noble
Magnesium	Lead
Magnesium alloys	Tin
Zinc	Nickel (active)
Aluminium 2S	Inconel (active)
Cad mium	Hastelloy C (active)
Aluminium 17 ST, Steel or iron	Brass
Chromium iron (active)	Copper
Ni-resist	Bronzes
18-8 Chromium -Nickel-Iron (active)	Copper -Nickel alloy
19-8-3 Chromium -Nickel- Molybden um-iron (active)	Monel
	Silver Solder
	Nickel (passive)
	Inconel (passive)
	Chromium ion (passive)
	18-8Chromium -Nickel-Iron (passive)
	19-8-3 Chromium -Nickel- Molybden um-iron (passive)
	Hastelloy C
	Silver
	Graphite
	Gold
	Platin um

Table 1: Galvanic Series Classification of Metals

In a not her case of galva nic corrosion, crack in mill scale on steel surface forms galvanic couple with underlying steel and the galvanic couple is strong enough to corrode the steel below. This effect is illustrated in Figure 1. Mill scale varies in thickness from 50 microns to 5000 microns and u su ally con sist s of ou ter layer of stable ferric oxide (Fe₂ O₃), in ter mediate layer of ferrosol-ferric oxide (Fe $_3$ O₄), and u n stable ferrou s oxide (FeO) as inner most layer intermingled with crystalline steel structure. The unstable FeO oxidizes to ferric st a te with increase in volum e resulting in loss of the scale layer exposing more steel surface to corrosion.

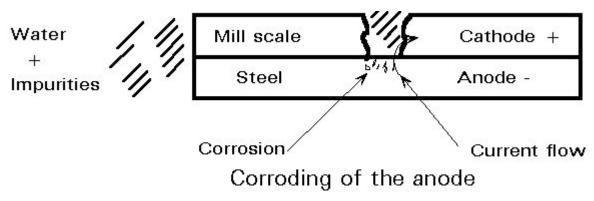


Figure 1: Corrosion Between Mill Scale and Steel¹

Concentration Cell

Severe corrosion, leading to pitting is often ca u sed by concen tra tion of cells partic ularly where t here are differences in dissolved oxygen concen tra tions. This type of corrosion is very common in industrial steel structures in contact with water relatively low in dissolved oxygen. The steel is anodic in a reas in contact with water with higher dissolved oxygen and cat hodic in areas with minimum oxygen contact. There can also be difference in metal ion concentrations in different regions of steel in contact with electrolyte that can lead to for mation of electrode pair. Metal from the anodic part disin tegrates from the matrix to increase ion concentration that manifests as corrosion. Typical examples are crevice corrosion due to jointing of metals or pits formed due to breakage of mill scale or coating voids. Schematic illu stration for the two types of concentration cell corrosion is presented in Figure 2.

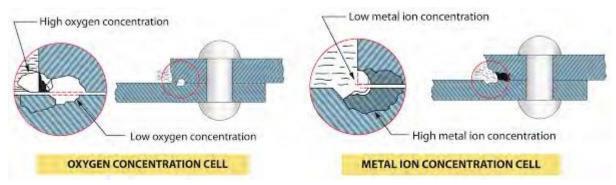


Figure 2: Concentration Cell Corrosion Mechanism¹

Other Forms of Corrosion

There a re m a ny ot hers for m s of corrosion all of which a re not disc u ssed in detail but a summarised list of corrosion mechanisms prevalent in industrial structures is presented in Table 2.

Sl. No.	Failure Mechanism-Rank	% of occurrence		
1	General Corrosion	25.8		
2	Fatigue or corrosion fatigue	18.7		
3	Stress Corrosion	11.7		
4	Erosion Corrosion	8.7		
5	Pitting	6.8		
6	Weld and fabrication defects	5.0		
7	Overload, mechanical abuse	4.2		
8	Brittle fracture	3.9		
9	Wrong material selection	3.4		
10	Wear	3.2		
11	High temperature oxidation or creep	1.8		
12	Casting flaws	1.6		
13	Crevice Flaws	1.6		
14	Intergranular corrosion	1.1		
15	Hydrogen Embrittlement	0.6		
16	Dissimilar metals	0.5		
17	Heat treatment errors	0.3		
18	De alloying	0.6		
19	Others			

Table 2: Corrosion Mechanisms for Steel Structures in IndustrialSettings

ENVIRONMENT/EXPOSURE CONDITIONS

As disc u ssed earlier, environment plays the gover ning role in initiating the corrosion. The designer tries to assess the environment al conditions before selection of specific paint system. All the environment al factors that are considered have one thing in common that is aqueous environment. Water is an important, sometimes a major constituent of such environment and plays a nessential part in the corrosion process that occ u rs. The first environmental factor taken up for discussion in this article is water.

Water

Nat ur al water is ultim a tely derived from sea water or from r ainwater. The com position of seawater varies especially near la rge est u a ries or a t differen t depths. The main controlling parameters are dilution or pollution (both from

rivers) and dissolved oxygen which varies with the depth and temperature. Rainwater usually has low probability of contact with metals except when it has a considerable bearing on atmospheric corrosion. Dissolved gases in water is another factor that controls the corrosion process. Carbon dioxide that rem ain s uncom bined in solution is a frequent source of corrosion for structures in contact with water. Dissolved oxygen is almost always present in sufficient q u a n tity to be im porta n t. Traces of a few parts per million oxygen in the purest of water can accelerate corrosion. It is the environment in the immediate vicinity of the metal surface that counts as far as corrosion is concerned.

In de- aerated n a tur al water, the rate of corrosion may be usually high due to the presence of sulp hate reducing bacteria in water. The bacteria only thrive in the absence of Oxygen and within the p H range of about 5.5 to 8.5. This type of corrosion of is generally seen in buried pipelines of deep-water wells and casing of oil Wells.

Soils

The next environment to which structures are exposed is soil. Here the water is held in the soil structure in many complex ways and contains a wide variety of corrosive ingredients. The soil it self may consist of sand, clay, ch alk, decomposed organic matters and other minerals / chemicals. The soil may be well aerated or relatively air free; the soil water level may be per manently above or below the buried metal. Further if the electrical resistivity of the soil is low, the localized corrosion will accelerate and spread due to low electrical resistance. The protection system by paints or coatings will not suffice - cat hodic protection by u sing impressed current or sacrificial anode in most cases are adopted along with other options.

Chemical Environment

There are endless variety of aqueous environments to which metals are exposed in process plants. The most common corrosion chemicals are acids, chlorides, salt, partic ularly oxidizing salt which take away the free electrons from metal surface and is difficult to prevent or stop completely.

Atmosphere

This is the most common environment to which plants and equipment are exposed in some form or other. Air itself is not particularly corrosive to the main structural metals. In clean air steel is attacked very slowly even if the air is moist. It would take 70 years to fully corrode steel plate of 3 millimeters thick ness if located in rural at mosp here and can go up to thou sand years in hot dry climates. In salt laden area in marine environments and especially in the immediate vicinity of the coast much higher rates of attack becomes common. Examples of these higher corrosion rates are given in Table 3¹.

Distance from Surface (metres), apprx.		Corrosion r a te micron s / yr. – Zinc	
50	38	1.5	11.1
200	15	0.6	3.1
400	2.2	0.1	0.8
1300	1.6	0.02	-0.2
3000	-	-	

Table 3: Atmospheric Corrosion Rate (Microns) for One-Year Exposureto Sea Salt⁶

Note: Salt contents expressed as mg NaCl/day/100 m² cloth area

The most serious cause of atmospheric pollution is from manmade polluting environment. Atmospheric pollution from burning of fossil fuels and from other industrial processes, makes all the structural metals corrode more rapidly. Presence of water in some form is necessary, even if the relative humidity is shown below 100 %, many common metals particularly iron and steel are found to corrode. It is certain that at a given temperature there is a critical humidity for metals such as steel, copper, zinc etc. above which corrosion is considerably increased especially when pollutants like SOx / NOx, and/or sea salts are present.

In summ ary, the designer must go in dept h for the correct assess ment of the environment in which designed metal atoms are exposed. The basic classes of environment are as listed below.

Dry Tropical Rural Humid Temperate Urba n Marine Arctic Industrial

A site can be a combination of these basic environment classes. In case of a structure located in marine tropical industrial environment it is easy to understandits corrosion severity. ISO 12944 classifies environment into five lasses based on the exterior condition and impact on structural components as shown in Table 4.

ROLE OF PAINTING IN CORROSION PREVENTION

The use of pain ts and in dustrial coatings is the most common way to con trol a large segment of the general atmospheric corrosion. Industrial paintings

can provide superior resistance against corrosive environment, chemicals, water, temperature, and abrasion.

Class	Impact	Interior	Exterior
C1	Very low	Heated buildings with clean air, s u ch as offices, s hops, schools, hotels, etc.	None
C2	Low	B uildings not heated, where condensation may occur, suchas warehouses and sports halls.	At mosp here wit h low pollu tion e.g., in t he country.
С3	Middle	B uildings for production with high at mosp heric humidity and some air pollution such as foodm anufacturers, breweries, dairies and laundries.	areas, moderate
C4	High	Chemical manufacturers, swimming bat h s a n d s hip- a n d boatyards by the sea.	In d u s trial a reas a n d coastal a reas wit h moderate salt impact.
C5-I	Very high - Industry	B uildings or a reas wit h almost permanent condensation and with high pollution.	
С5-М	Very high	B uildings or a reas wit h almost permanent condensation and with high pollution.	

Table 4: Corrosion Class and Environment (Internal/External

Action of Paint

Paint is a mixture of pigment which gives opacity and a liquid binder material (vehicle) which binds the pigments together. The purpose of paint coat is to protect the metal surface from its environment.

Paint retards the corrosion of steel in number of ways:

i. Paint forms more or less an impervious barrier between the metal surface and the surrounding environment. This mechanical barrier is not totally impervious. Even with the best paint products and best met hod of application there will be pores through which moist ure a n d air / gases will diffu se to corrode t he metal. Therefore, application of multiple coats is adopted to hin der t he diffu sion process.

- ii. It is well k nown that certain chemical com pounds either completely stop or retard the corrosion of the steel. It is understood that these com pounds form films on the anodic or cathodic area which lead to the suppression of the corrosion. For example, chromate salts can easily be leached away; therefore, less soluble zinc chromate pigments find use as rust inhibitor. Zinc phosphate pigment which is occupation ally safest rust inhibitor pigment is used extensively for primer paint for mulation s. Similarly, red lead (lead oxide) pigment when dispersed with lin seed oil and alloyed to dry form lead soaps which form a dense rough film of very low water permeability.
- iii. Corrosion is an electrochemical process where electric current from anode (corroding metal) to cathodic area or environment causes metal to corrode away. Paint films formed due to polymerisation of orga nic vehicle act as in sulating mem bra ne which disr upts the flow of electrical current if the film is intact.

In summ ary, it might be stated that a suitable metal protective paint must be one with rust inhibitive properties, low per meability to corrosive agents, low absorption of water and the ability to wet the surface to which it is applied. In special cases the paints hould have fire retardant properties when the installation is prone to fire hazard.

Performance of Paint System

The important factors which govern the desired performance of an industrial paint system are:

- i. Proper design of the structure / equip ment to be painted and the appropriate selection of the material which can with stand the environment. If the selection of basic engineering material is in appropriate with respect to the environment, the paint alone cannot protect the metal; paint at best retards the corrosion rate but cannot stop the process.
- ii. Correct assessment of the likely exposure conditions and the operating temperature of the surface to be painted. Corrosion rates generally increase with rise in temperature, but presence of oxygen also plays crucial role in controlling the rate⁷.
- iii. Location of the structures/equipment indoor or outdoor installation.
- iv. Whet her the structure/equip ment are underground or over ground or immersed in water; in case of immersion in water, the water quality and existence of any splashing zone where the structure undergoes alternate cycles of wetting and drying need to be assessed.
- v. Selection of specific paint system for specific environmental consideration.
- vi. Proper surface preparation and formulation and application of paint
- vii. Monitoring of paint condition and timely maintenance of painting by touch-up and re-painting.

CORROSION IN STEEL PLANT AND CORROSION PROTECTION COATING SYSTEM

The following case study is from a typical environment in Steel Plant. Table 5 identifies the plant area, corrosion zone and the corrosion rate. Steel plant atmosphere have high dust loads and these tend to settle on structural mem bers. The acc umulated dust contain spollu ting chemicals and absorbs moisture from air or gets wet in rain. This mixture aggravates the corrosion process in the steel structure. Table 6 shows anticipated dust accumulation in various areas of steel plant.

SI. No.	AREA / PLANT	ZONES	Corrosion Rates (mils per year)
1.	Rolling Mill a rea, Engg. Work S hops, Raw Material Area		Corrosion rate less than 1 mpy
2.	E.T.P. Area, SMS Area, Captive Power Pla n t Area		Corrosion rate between 1 & 3 mpy
3.	Coke Oven area, Coke Plant By-Product Area	Corrosive Zone.	Corrosion rate between 3 & 5 mpy
4.	Pig Casting Machine Area, Pickling Mill area.	Highly Corrosive Zone.	Corrosion rate of 5 mpy & above

 Table 5: Areas of Steel Plant with Corrosion Rates

Paint System

A paint film forms only mechanical bondage with the virgin metal surface. The surface should be artificially prepared to provide anchoring profile for the paint film. Application of paint on the rusted metal surface or on greasy surface the paint will not hold. Up to 70% of coating failu re have been bla med on poor surface preparation. There are variou s methods of surface preparation like wire brushing, power tool cleaning, or shot blasting, chemical cleaning (pickling) that is quickly and even flame cleaning depending on degree of cleanliness desired. degree of cleanliness of Steel surface represents as St. 1 to St. 3 and Sa1 to Sa3 are pictorially represented in Swedish Standard S/S 055900.

The anti-corrosive paint system comprises of following:

Prime Coat

Prime coats are the initial basic coats to be applied preferably by brush on the fres hly prepared steel surface. Primers provide ad hesion to the metal plus corrosion control to protect it. There are three main types of primers

> barrier primers inhibitor primers zinc rich primers

DUST DEPOSI				Γ
Location Type Dust		Deposition rate per year (Thick ness in mm)	Den sity (Kg/Cu.M)	Remarks
SMS	Iron	75 mm and more	1700	Irone Fines
Lime Calcining Plant	Lime	100 and more	1300	Lime, Dolo etc
Sinter Plant	Sinter	100 mm and more	1850	Sinter Mix
Captive Power Plant	Coal / As h	50mm and more	870 1000	Coal Dust Fly Ash
Blast Furnace	Iron Ore / Sin ter	300 mm and more	2400 1850	Iron Ore Sinter
Raw material	Iron	75 mm and more	1700	Variou s Raw Materials including Iron
Coke Ovens	Coal / Co ke	300 mm and more	870 750	Coal Dust Coke Dust
Note:	1		1	1
1 Table	for med ba	sed on experience a	and various	in teractions

 Table 6: Dust Deposition in Steel Plant Areas

. . Table for med based on experience and various interactions with plant personnel

2 . The acc umulated thick ness is in dicative, can be bettered with proper maintenance

Barrier primers are imper meable films such as vinyls, chlorin ated rubber, epoxies etc. these primers reduce the access of water, chlorides, and s ulp h a tes to t he Steel. They im part corrosion resista nce by a rtificially increasing t he electrical resista nce of t he corrosion cell. Barrier primers a re most favou red where t here is con tin uou s expos u re to corrosive electrolytes such as Marine installations, chemical installations, water storage tanks or buried pipelines.

Inhibitive primers a re commonly com posed of oil base, alkalyds of p henolic alkalyd vehicle that contains small additions of soluble inhibitors such as ch rom a tes, molybdates etc. These inhibitor chemicals dissolve as moist u re diffu ses t h rough t he pain t system to the Steel s u rface. The inhibitor t hen retards t he electrochemical corrosion reaction s at t he microscopic a nodic or cathodic areas on the steel surface. Zinc rich primers a re highly loaded with metallic zinc e.g., 86 % by weigh t. The zinc sacrificially corrodes to protect the steel which acts as noncorroded cathode. Zinc-rich Primers protect against corrosive undercutting of paint system and in additions offers good abrasion resistance.

There are ot her organic (e.g., epoxy) and inorganic (e.g., ethyl silicate) zinc rich primers. Organic zinc rich primers can tolerate slightly poorer surface preparation quality and easier to apply than inorganic ones. chemical resistant wise organic zinc rich primer is better than inorganic based. However, dry heat resistance for organic primer is limited to 120° Celsius to 150° Celsius for the inorganic primers.

In outdoor exposure or other environment, essentially in neutral pH con dition t he inorga nic zinc primers can be left without top finis h coat (ignoring aest hetics). However, if t he pH of t he environment is below 5 or above 10, un top-coated zinc rich increase primers a refavou red for shop priming of steel t h at is slated for use in severely corrosive environment s u ch as con tin uou s or in termittent t immersion of seawater or for long ou tdoor life. Zinc rich primers h ave been called the "ultim ate con tribution of the paint technologies to the work on corrosion".

Top Coat

The role of the topcoat is to

- I. protect the primers from weathering
- II. provide the protection as listed in the Table 7^8
- III. provide aest hetics including long lasting colour and gloss preferably without excessive chalking, fading, or yellowing.

Relative resistance of different types of top quotes against various types of environment is given in Table 7.

Paint Film Thickness

Enough paint must be applied for corrosive environment and is usually a minimum of three coats with the total dry film thick ness that is DFT of at least 125 microns. In one comparison for structures in steel plant exposure, it is reported that oil-based coatings of 100 to 125 micron give 8 to 10 years of protection in rural environment whereas for marine environment the coating need to build more, minimum 220 micron s for oil-based pain t, 125 microns for alkalyds, 115 microns for epoxy and 120 microns for chlorin ated rubber and 75 micron for vinyl if 8 to 10 years protection are desired.

High B uild coatings of t hick ness DFT 50 to 75 micron s per coat provide a n economical mea n s of adding more micron s for application b u t a re not as protective as regular build coating applied in several coats to give an equivalent film thick ness.

Compatibility of Paint System

This is a very important aspect while recommending a paint system. All paints are not compatible which means by selection of any specific paint as a primer the top coat cannot be chosen at random. With alkali primer epoxy

top coat is not compatible as if it will chemically decompose the epoxies. There are similar such incompatibilities with many paints.

Paint	Acids	Alkalis	Salts	Solven ts	Water	Weather	Oxidation	Abras ion
Oil Based	1	1	6	2	7	10	1	4
Alkyd	6	6	8	4	8	10	3	6
Chlorin a ted rubber	10	10	10	4	10	8	6	6
Coal tar epoxy	8	8	10	7	10	4	5	5
Epoxy - amine /amide	9	10	10	9	10	8	6	6
Silicon Alkyd	4	3	6	2	8	8	6	6
Vinyl	10	10	10	5	10	10	10	7
Ureth ane	9	10	10	9	10	8	9	10
Zinc (inorganic)	1	1	5	10	5	10	10	10

Table 7: Relative resistance of common topcoat paints to exposure⁸

Note: A value of 10 represents the best protection.

Specifying a suitable painting system for steel structure should address the following aspects at minimum:

- 1. assessment of the environment
- 2. selection of right paint system
- 3. surface preparation standard
- 4. method of application including number of coats / paint thick ness
- 5. drying time and coating intervals
- 6 . crucial application limitations
- 7. . strict observance of the maker's

direction s8. safety precautions

- 9. . cleanup
- 10. . in spection and quality control

Paint Failure

Despite design and application of the best paint system the paint film is susceptible to fail for various reasons some of which are listed below.

i) Faulty mechanical design of the structures and equipment by which the surface contours are such that uniform coating thick ness cannot be developed.

- ii) Im proper application of pain t, most of the defects in a n applied pain t which do not s tem from im proper s urface preparation bu t from incorrect mixing of pain t ingredien ts or application in a hurry without waiting for drying.
- iii) Incorrect paint formulations or old paints in use
- iv) Loss of adhesion
- v) Application of paint in humid weather
- vi) Mechanical stresses and other abuses on the paint film
- vii) Un der film corrosion t his occu r s most readily when t he coated metal is exposed in high humidity environmen t (50 200 % R.H>) and sit u a tion becomes worse if t he environment is saline as in the case of m a rine environment. It can be retarded if t he relative humidity of t he environment t is maintained at less t han 50 %, if an inhibitor is added to t he pain t or if t he reactivity of t he metal s u rface is decreased by means of metal surface treatments that form on the substrate metal a com pound of t he metal (e.g., a p hosph a te or a n oxide) t hat is less reactive than the bare metal.

It is thus mandatory to chalk out a regular paint and structure health in spection pla n and carry out periodic checks and main ten ance of the paint coatings throughout the service life of the structure.

MAINTENANCE OF PAINTING

If the engineering structures and equip ment need to be protected from corrosion, the protection measures adopted need equal maintenance care as plant and machinery. It is more important to have regular maintenance on retaining the pain t film than to replace the entire metal badly affected by corrosion.

In all maintenance painting the aim is to repaint before the old paint has deteriorated to a stage where it must be entirely removed. This is done by periodically applying a single new coat of paint over the cleaned old paint substrate. The nor mal span of such a period for a marine in stallation should be around 2 years both for outside and inside painting if required.

In maintenance painting it is not intended that sound, adherent old paint system be removed unless it is excessively thick or brittle or is incompatible with the new paint. However, the defective paint layer shall be removed beyond the edges of the defect spot or area till a zone of intact and perfectly ad heren t paint layer withou trustor blister below the film is reached. The retained part of old paint zone should have adequate adherence to prevent it getting lifted as a layer when putty k nife is in serted under the coating. The edges of adherent paint coat outside the defective area are feathered to create a gradual taper towards the zone of recoating to create smooth overlap zone. For defective areas of old paint substrate, work involves spot cleaning to provide new anchoring profile and application of adequate number of coats of compatible primer over those areas is carried out to build them up to a satisfactory level. Then a noverall finis h coat is applied as fin al coat. Today everybody is aware t h at timely remedial meas u res again s t corrosion would not only save the h uge expendit u re in replacing the corroded defunct equip men t/s teel s truct u re by new one but also of the production s h ut down time can be reduced. In recent times computers have been deployed to com pile system a tically all sorts of corrosion data, results of corrosion preven tive meas u res and predict fut ure plan of action to com bat the corrosion.

CONCLUSIONS

Steel / Steel Structure is subjected to degradation by corrosion. Corrosion is a n a t u r al p henomenon which occu r s in simulta neo u s presence of water a n d oxygen (air). However, rate of corrosion is not unifor meverywhere. There are several factors which influence the rate of corrosion. Rate of corrosion can be minimized but can't be eliminated. Corrosion is controlled by changing t he environmen t, though it is diffic ult. Rat her it is easier when protective system is adopted. Pain ting is the best met hod of preven ting corrosion in steel structure. However, its effectiveness is depending on many factors. However, steel structure can last more than 100 years with application of proper protective maintenance painting.

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HIGH STRENGTH STRUCTURAL STEEL

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INTRODUCTION

Steel, Concrete and Wood are the three popular materials for constructing structure such as Bridges, Buildings and Stadiums etc. Steel is preferred for its high strengt h to weight ratio. Concrete is popular for its easy availability in small quantity and easy casting proced ure. Woods are becoming scarce now-a-days.

Steel is a very important material for making structure. Because of its high strengt h to weight r a tio, steel structure is slim and elegant. It occupies less space and offer high durability. Mild steel (yield strength <350 MPa) is the most common type of steel used for making structure. Obviously, more the strength of steel, more elegant is the structure. However, this concept does not match with the Indian construction scen ario. High strengt h steel (yield strengt h > 400 MPa), though popular in developed countries, is comparatively new product in India. Highs trengt h low-alloy s teel (HSLA) s teel is an alloy s teel t h at provides better mech anical properties or greater resista nce to corrosion than carbon steel. HSLA steels are not made to meet a specific chemical composition but rather to specific mechanical properties.

Steel is strong in ten sion requires special arra ngement of sections when it is subjected to compression. Concrete is strong in compression but very week in tension. Steel Reinforcement is given in concrete when it is subjected to tension. In this case, concrete is better known as Reinforced Concrete (RCC).

Steel is produced in industry and it is compound materials. Ensuring q u ality in s teel is easier. Concrete is mixed m a terials prone to non-homogeneity of quality.

Steel, being a compound and industry made products offer wide variety of properties and applications – both structural and non-structural.

STEEL

Steel is an alloy of Iron and Carbon. But it has alloying elements such as Manganese, Phosphorus, Silicon and Sulphur. Many other alloying elements are added for achieving any specific property required for a particular application.

STRUCTURAL STEEL

Steel, when used to construct structure, is known as Structural Steel. Yield Stress, Maximum Tensile Stress, Elongation, Toughness and Weldability are important properties of steel. Addition of Carbon in to steel increases the strength of steel but it decreases elongation and weldability. This phenomenon limits the strength of steel for structural application.

Structural Steel in India has been specified mainly by following two codes / standards:

- 1. IS 15911 : 2010 [Structural Steel (Ordinary Quality) Specification]¹
- 2 . IS 2062 : 2011 (Hot Rolled Medium and High Tensile Structur al Steel Specification) 2

Chemical Compositions and Mechanical properties of different grades of structural steel are given in Table 1, Table 2, Table 3 and Table 4.

Table 1: Chemical Composition of Structural Steel as per IS 15911 :2010

Sl No.	Grade Designation		Ladle Analysi	Ladle Analysis, Percent, Max			
		C	Mn	S	P		
(1)	(2)	(3)	(4)	(5)	(6)		
i)	E165		1.0		1.1		
ii)	E170 >	0.25	1.25	0.060	0.075		
iii)	E215						

Table 2: Mechanical Properties of Structural Steel as per IS 15911 –2010

SI No.	Grade Designation	Tensile Strength R _m Min MPa	Yield Stress R _{eff} Min MPa	Percentage Elongation, A at Gauge Length, L_o $5.65\sqrt{S}_o$ Min	Internal Bend Diameter
(1)	(2)	(3)	(4)	(5)	(6)
i)	E 165	290	165	23	21
ii)	E 170	330	170	23	31
iii)	E 215	370	215	23	31

It has been observed that structural steel having strength range from 165 N/mm^2 to 650 N/mm^2 have been specified in the standards.

In addition to above -men tioned two standards, a not her two standards of structural steel are published for specific application as mentioned in the

respective title but these are in lesser use as these are not included in the IS: 800 - 2007 (General Construction in Steel - Code of Practice)³ overtly.

- IS 11587 1986 (Specification for Structural Weather Resistant Steels)⁴
- 2 . IS 15103 2002 (Fire Resistant Steel Specification) ⁵

In the above-mentioned two standards, structural steel of strength range from 240 N/mm² to 350 N/mm² has been specified.

Table 3: Chemical Composition of Structural Steel as per IS 2062 :2011

Grade Designation	Quality		Ladl	e Analysis, P	ercent, Max	1.17	Carbon	Mode of Deoxidation
Designation		С	Mn	S	Р	Si	Equivalent (CE), Max	Deorination
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
	A	0.23	1.50	0.045	0.045	0.40	0.42	Semi-killed/killed
E 250	BR B0	0.22	1.50	0.045	0.045	0.40	0.41	Semi-killed/killed
	C	0.20	1.50	0.040	0.040	0.40	0.39	Killed
	A	0.23	1.50	0.045	0.045	0.40	0.43	Semi-killed/killed
E 275	BR B0	0.22	1.50	0.045	0.045	0.40	0.42	Semi-killed/killed
	С	0.20	1.50	0.040	0.040	0.40	0.41	Killed
E 300	A BR B0	0.20	1.50	0.045	0.045	0.45	0.44	Semi-killed/killed
	C	0.20	1.50	0.040	0.040	0.45	0.44	Killed
E 350	A BR B0	0.20	1.55	0.045	0.045	0.45	0.47	Semi-killed/killed
	C	0.20	1.55	0.040	0.040	0.45	0.45	Killed
E 410	A BR B0	0.20	1.60	0.045	0.045	0.45	0.50	Semi-killed/killed
	С	0.20	1.60	0.040	0.040	0.45	0.50	Killed
E 450	A BR	0.22	1.65	0.045	0.045	0.45	0.52	Semi-killed/killed
E 550	A BR	0.22	1.65	0.020	0.025	0.50	0.54	Semi-killed/killed
E 600	A BR	0.22	1.70	0.020	0.025	0.50	0.54	Semi-killed/killed
E 650	A BR	0.22	1.70	0.015	0.025	0.50	0.55	Semi-killed/killed

HIGH STRENGTH STUCTURAL STEEL

Structural steel having Yield Strengt hmore 400 MPa is understood to be High Strength structural steel. As high strength steel is preferred to for construction of structure with the assumption that structure built with high strength steel will make self-weight of structure comparatively less and it will result into cost of structure cheaper. But this simple assumption may not be true always because price of high strength steel is more com paratively. There a re technical reason s too for limited u se of high strength steel. It is described here.

Deflection of mem bers of structure is limited by the Clause No. 5.6.1 (Limit State of Serviceability) of IS 800 - 2007 which is some fraction of lengt h / height of mem ber. For mula used for calculation of deflection indicate that amount of deflection does not depend on strength of material. It increases when Load Applied and Lengt h of member increase a n d it decrease when Momen t of Inertia a n d Mod ulu s of Elasticity increase. Mod ulu s of Elasticity for s teel is ass um ed to be con s t a n t irrespective of s trengt h of s teel. Therefore, high s trengt h of s teel is not effective for using when it is restricted by Deflection Limit.

Therefore, high strength steel should be used where deflection is not the limiting criteria. Use of high strength steel is advantageous where members are subjected to only tensile stress – commonly understood as Tensile Structure.

Grade Designation	Quality	Tensile Strength R _m , Min MPa ⁽¹⁾		Yield Stres R _{ett} , Min MPa ¹¹	S	Percentage Elongation <i>A, Min</i> at Gauge Length,	Internal Bend Diameter Min (See Note 2) ≤ 25 >25		Chai Impact (See No	Test ote 3)
	-	(See Note 1)	<20	20-40	>40	L_=5.65			Temp °C	Min J
(1) (2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	
E 250	A BR B0 C	410	250	240	230	23	2t	3t		27 27 27 27
E 275	A BR B0 C	430	275	265	255	22	2 <i>t</i>	3t	 RT 0 (-) 20	<u> </u>
E 300	A BR B0 C	440	300	290	280	22	2t	-	 RT 0 (-) 20	27 27 27 27
E 350	A BR B0 C	490	350	330	320	22	2t		 RT 0 (-) 20	27 27 27 27
E 410	A BR B0 C	540	410	390	380	20	21	-	 RT 0 (-) 20	25 25 25
E 450	A BR	570	450	430	420	20	2.5t			20
E 550	A BR	650	550	530	520	12	3 <i>t</i>	-	 RT	15
E 600	ABR	730	600	580	570	12	3.5t	-	RT	15
E 650	A BR	780	650	630	620	12	4t	-	 RT	15

Table 4: Mechanical Properties of Structural Steel as per IS 2062 –2011

WELDABILITY OF HIGH STRENGTH STUCTURAL STEEL

In addition to the restricted u se of high s trengt h s teel ca u sed by limited deflection, weldability is a not her deterren t for u sing high s trengt h s teel in structure.

In 1940, Dearden and O'Neil⁶ have recommen ded the relationship between chemical compositions of steel and hard ness of steel in the HAZ after welding. This is given by:

Maximum Vickers Hardness Number (H_V) = $1200CE_{Dearden} - 200$ Where, Carbon Equivalent (CE _{Dearden}) = $C + \frac{P}{2} + \frac{Mn}{6} + \frac{Cu}{13} + \frac{Ni}{15} + \frac{Cr}{5} + \frac{Mo}{4} + \frac{V}{5}$

It is believed t h a t if HAZ h ard ness of s teel is less t h a n 350 HV, no coldcracking would occur after welding but if the HAZ h ard ness is greater t h a n 400 HV, t he s teel would be prone to cold-cracking. It is k nown t h a t welding is very important joining method for constructing a steel s tr u ct u re. Weldability is t he ease of welding by with two members can be joined without any crack or any other defect.

In 1970, Bastien ⁷ has found the relationship between critical cooling rate, CR_M (maximum time required by unstable austenite to be transformed into martensite) and carbon equivalent as given below:

$$ln(CR_M) = 13.9 - 10.6 CE_{BastBBen}$$
$$CE_{BastBBen} = C + \frac{Mn}{4.4} + \frac{NN}{10.3} + \frac{Cr}{15 \cdot 4} + \frac{Mo}{7 \cdot 7}$$

It should be noted that welding in structure is carried out in hot condition (more than 723 °C temperature) which allow re-crystallization in steel. Quick cooling helps to form Mertensite micro-structure which has hard ness of more than 400 HV, indicating the welding is prone to crack during service of the structure.

Therefore, it is concluded that Carbon Equivalent is indicator of weldability of steel.

It is experienced by welding personnel t h a t if Carbon Eq uivalen t (CE) is more t h a n 0.45, t he steel is very difficult to weld. In t his case, Carbon Equivalent is calculated by the following formulae.

$$CE = C + \frac{Mn}{6} + \frac{Cr + Mo + V}{5} + \frac{N\mathbb{H} + Cu}{15}$$

Carbon Equivalent of E410 Grade steel produced as per IS 2062 - 2011 is 0.50. Therefore, welding of this steel is difficult. Difficulty in welding of high strength steel can be eased a little by following methods:

Preheating of steel before welding

Slowing the Post-Welding-Cooling to such a level that microstructure of steel would be anything other than Marten site.

Micro-alloying of steel in such a way that Carbon Equivalent of steel will be less than 0.5.

O ut of t he t h ree met hods men tioned above, Preheating of s teel a n d lowering t he post-welding cooling r a te depend on t he skill of welder as well as the works hop / environment where the welding is being carried out.

However, t he problem can be solved in a better way if High Strengt h Low Alloy Structural Steel is produced with lower Carbon Equivalent.

HIGH STRENGTH LOW ALLOY STRUCTURAL STEEL

IISI (International Iron and Steel Institute) classify the steel as High Strength Structural Steel when the structural steel contains maximum 0.2% carbon and up to 2.5% alloying elements by weight.

Str u ct u r al Steel h aving more t h a n 400 MPa Yield Strengt h specified in IS 2062 - 2011 is not tr uly High Strengt h Low Alloy Steel as per IISI classification. However, m a ny t hin k t h a t t he High Strengt h Steel is micro-alloyed because of Note No. 5 and Note No. 6 given in the code as stated below:

Note No.5 Micro-alloying elements like Nb, V and Ti may be added singly or in combination. Total micro-alloying elements shall not be more than 0.25 percent.

Note No.6 Alloying elements such as Cr, Ni, Mo and B may be added under agreement between the purchaser and the manufacturer. In case of E 600 and E 650 the limit of Cr and Ni, either singly or in combination, shall not exceed 0.50 percent and 0.60 percent respectively.

As bot ht he Notes make the micro-alloying option al, no high strengt hmicroalloyed steel is prod u ced in In dia in reality. In In dia, h ardly there is a ny scope for a con sum er to disc u ss about the chemical composition of s teel with producers.

In this context, EN 10025^{8,9,10,11,12,13}, the standards for specification steel can be referred to. It has six parts with following descriptions:

- Part 1: Hot rolled prod u cts of s tr u ct u r al s teels General technical delivery condition
- Part 2: Technical delivery conditions for non-alloy structural steels
- Part 3: Technical delivery con dition s for nor m alized / nor m alized rolled weldable fine grain structural steels

- Part 4: Technical delivery con dition s for t her mo-mech a nical rolled weldable fine grain structural steels
- Part 5: Technical delivery conditions for structural steels with improved atmospheric corrosion resistance
- Part 6: Technical delivery conditions for flat products of high yield strength structural steels in the quenched and tempered condition

It can be seen that classification and specification of steel are easily understandable and more scientific. Steel specified in Part 2 of EN 10025 is non-alloyed but steel specified in Part 3 of EN 10025 is micro- alloyed steel. High Strength steel specified in Part 3 is weldable and weldability has been im proved because it is fine grained steel. The chemical com position and mech a nical properties of steel specified in EN 10025 (Part 3) are given in Table 5 and Table 6 respectively.

Table 5: Chemical Composition of Structural Steel Specified in EN
10025 – 2004 (Part 3)

Desig	nation	C % max.	Si % max	Mn %	P % max.	S % max.	Nb % max.	V % max.	Al _{total} . % min.	Ti % max.	Cr % max.	Ni % max.	Mo % max.	Cu % max.	N % max.
According EN 10027-1 and CR 10260	According EN 10027-2	F													
S275N	1.0490	0,18	0.40	0,50 - 1,50	0,030	0,025	0.05	0.05	0.02	0.05	0.30	0.30	0,10	0.55	0,015
S275NL	1.0491	0,16	0,40	0,00 - 1,00	0,025	0,020	0,00	0,00	0,02	0,05	0,50	0,50	0,10	0,00	0,015
S355N	1.0545	0,20			0,030	0,025	0.05							0,55	0,015
S355NL	1.0546	0,18	0,50	0,90 - 1,65	0,025	0,020	0,05	0,12	0,02	0,05	0,30	0,50	0,10		
\$420N	1.8902				0,030	0,025	0.05				0,30	0,80			0,025
S420NL	1.8912	0,20	0,60	1,00 - 1,70	0,025	0,020	0,05	0,20	0,02	0,05			0,10	0,55	
S460N e	1.8901 ^e			0,60 1,00 - 1,70	0,030	0,025	0.05					0,80	0,10		0,025
S460NL ^e	1.8903 ^e	0,20	0,60		0,025	0,020	0,05	0,20	20 0,02	0,05	0,30			0,55	

Steel gets cooled as it is rolled, with a typical rolling finis hing tem perat u re of a roun d 750°C. Steel is then allowed to cool n a t u r ally is ter med 'as-rolled' steel a n d "As Rolled" Str u ct u r al Steel is specified in Part 2. Nor malizing takes place when as-rolled material is heated back u p to approximately 900 °C, and thenheld at that temperature for a specific period time, before being allowed to cool n a t u r ally. The process of nor malizing refines the grain size of steel and improves the mechanical properties, specifically toughness and improves weldability as well.

The process for Quenched and Tempered steel starts with a normalized material at 900°C. It is rapidly cooled or 'quenched' to produce steel with high strength and hardness, but low toughness. The toughness is

restored by reheating it to 600°C, m ain t aining t he tem perat u re for a specific time, and then allowing it to cool naturally (Tempering).

Table 6: Mechanical Properties of Structural Steel Specified in EN10025 - 2004 (Part 3)

Design	Designation Minimum yield strength Ren [®]						Tensile strength Rin.* MPa ^o			Minimum percentage elongation after fracture*								
	Nominal thickness mm					Nominal thickness			L₂ = 5,65 √3₀ Nominal thickness mm									
According EN 10027-1 and CR 10260	According EN 10027-2	s 16	≥16 ≤40				⇒ 100 ≤ 150	≥ 150 ≤ 200	> 200 ≤ 250	± 100	≠ 100 ≤ 200	> 200 ≤ 250	s 16	≈16 ≲40	*40 5 63	⇒ 63 ≤ 80	⇒ 80 ≤ 200	⇒ 200 ≤ 250
5275N \$275NL	1.0490 1.0491	275	265	255	245	235	225	215	205	370 to 510	350 to 480	350 to 480	24	24	24	23	23	23
8355N 8355NL	1.0545 1.0548	355	345	335	325	315	295	205	275	470 to 630	450 to 600	450 to 600	22	22	22	21	21	21
\$420N \$420NL	1.8902 1.8912	420	400	390	370	360	340	330	320	520 to 680	500 to 650	500 to 650	19	19	19	18	18	16
9460N 8460NL	1.8901	460	440	430	410	400	380	370		540 to 720	530 to 710	÷	17	17	17	17	17	4

CONCLUSION

High Strengt h Str u ct u r al Steel m ay be u sed wit h proper design to get advant age of high strengt h. Weldability is a deterrent for it s u se. To make the high strengt h steel, welding skill and infrastr u ct u reneed to be im proved on fabricator's part whereas producing the high strengt h steel with proper alloying is the responsibility of steel producers.

Before all of t hese to h appen, B u rea u of In dia n Sta n dards needs to revise all relevant standards.

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EFFICIENT CONSTRUCTION WITH STEEL WELD MESH FABRIC

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INTRODUCTION

Construction sector is one of the fastest growing sectors in the world con trib u ting la rgely towards in d u s trial and economic growt h. Observing similar stature in India, it is considered as one of the core industries con trib u ting significan tly to the economy of In dia. In the last decades the sector h as s hown an unpreceden ted change from convention al met hods to moder nised met hodology. Withhelp of advancements in civil engineering construction, solutions, and applications, the shift towards advanced technology and awareness towards eco-frien dly prod u cts h ave created a new perspective and acceptance amongst the end-users. The constant rise in dem and for progressive ease of construction solution s is shaping the future. Steel has been an integral part for all types of constructions for decades now. It su niq u eness lies in the fact that it reinforces the concrete which protects the construction structure from easy wear and tear that can occur from rust or any natural calamity like an earthquake. Reinforced concrete is the number one medium of construction. It is important to have good quality concrete and reinforcing bar (rebar). It is equally important to have competent bond between rebar and concrete. Reinforced Concrete Construction which is the backbone to any infrastructural project depends perfor mance prime elements namely Concrete for it s on it s and Reinforcemen t. Just as mech a nization of concrete prod uction n a mely Mix design, Au to batching plants, Ready Mix technology and au tom a ted casting techniques have raised the standards and strengths of concrete to rem arkable levels, the same is essen tial for reinforcemen t. Usage of Welded Wire Fabric (WWF) is the easy and correct solution for achieving the req uirements of quality, reliability, speed and efficiency is a prefabricated reinforcement consisting of a series of parallel longit u din al wires with acc ur a te spacing welded to cross wires at the required spacing. 2 Using weldedwire reinforcement as an alter native to tradition al mild steel reinforcing bars has many advantages. Weld Mesh is manufactured in square or recta mesh from steel wire, spot welded at eachin tersection. This is ngular one of the most versatile of in dus trial wire products and has inn um erable application sthroughout all types of industry. It is generally manufactured in mild galva nized and st ainless steel in differen twidt h, size and gauge. Weld Mes h is also used as rebar in reinforced concrete, graded sloped floor, false ceilings, poultry, warehouses for creating division s, shelfs, mines, gardening, machine protection and ot herdecorations etc

MATERIALS

Generic weld mes h m a terials are Mild steel, SS 304, SS 316 and galva nised for corrosion resistance. The reinforcing steel wires or bars which are used to reinforce concrete and masonry structures, enabling these to retain their tensile strength through changes in temperature, weather etc. Weld wire mes h h as higher yield strengt h and is prod u ced u n der higher quality con trol standards. Cold reduced wires which are plain, ribbed and indented surface configurations steel wire as shown in Fig.1 and Fig.2 with strength grades 500 N / mm 2 and 550N / mm 2 , u sed for the manufact u re of wire mes h for reinforcement of concrete. Mes h is made as per IS 432-2 grade steel with low impurities and for better welding. These wires are cold reduced from wire rods bv passing them through dies / rollers which provide ribs/indentations in the process. Cold reduced wires have less weak areas and provides for better bonding with concrete as can be provided with ribs / in dentations. Also, due to uniform microstructure of cold reduced wires, issues of weak welded joints are also reduced in these wires.

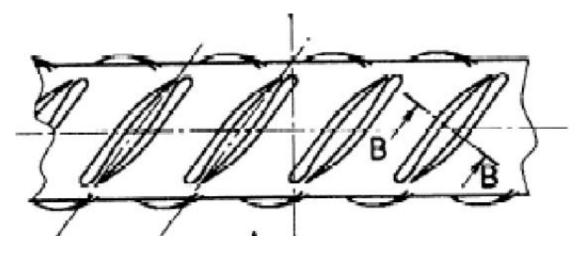


Fig.1: Ribbed Wires or Bars with Three Rows

The wires are covered in IS 432 (Pt 2) Specification for mild and medium ten sile steel bars and hard-drawn steel wire for concrete reinforcement. While hot rolled steel wires manufactured through controlled on-line cooling process are covered in IS 1786: High strengt h defor med steel bars and wires for concrete reinforcement. Further, use of these wires results in steel saving d u e to increased yield strengt h of cold red u ced wires th an hard-drawn plain wires and that of hot-rolled steel wires.

Torkari steel (cold twisted defor med) is mostly u sed as reinforcement bar (rebar) for the concrete in the construction. The steel contains higher strengt h (50 and 55 grade) and economic advant ages over the predecessors TOR- 40 (40 grade steel). Due to higher strengt h, it is cost effective. CTD bars however suffered from one disability as it became harder than mild steel during twisting operation and its ductility property reduced. Elongation at breaking point of CTD bars reduced to 14% as compared to 24% of Mild steel. Many times, cracks appeared on outer surface of CTD bars while making hooks. It was considered not very suitable to face reversal of stresses an in case of machine foundation or high-rise structures subjected to eart hq u ake or s trong win d. Ther mo Mech a nically Treated (TMT) bar, also called as Reinforcing Bar or Rebar is a high-strengt h reinforcement bar with a tough outer core and soft inner core made as per IS 1786. TMT steel bars a re a new generation of s teel bars for concrete reinforcement which is very widely used in present day construction work. Earlier CTD bars i.e cold twisted deformed bars were being used. Prior to that M.S or mild steel bars were in use for R.C.C (reinforced cement concrete) construction works. Rebar is u s u ally made from high-carbon tem pered s teel and it may be tied together in cross patterns for further reinforcement, and is cast with a ridged surface to aid in adherence to the concrete. 4 The fabric is formed by spacing the main and the cross wires, which shall be fixed at their pointy of intersection by electric welding, so as to be sufficiently stable to withstand nor mal handling in transport and during concreting, without displacement beyon dt he limits specified. Fabricated and finis hed mes h fabricated and finis hed will ass u re acc u r a te spacing and alignment of all mem bers of the finished fabric to give substantial square or rectangular openings.

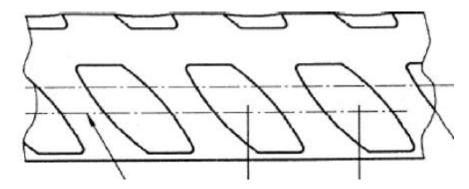


Fig.2: Intended Wires or Bars with Three Rows

STANDARDS & MANUFACTURING

Depending upon design the reinforcement wires / bars may be Cold Drawn Plain Wires, Cold Rolled Ribbed / Deformed Wires or Hot Rolled TMT Bars. Major manufact urers are processing cold drawn plain Wires and cold rolled ribbed / deformed Wires and limited manufacturers are processed with TMT rebars. These require initial Raw material MS Wire Rods of SAE-1008 / 1010 / 1015 or 1018 grades (with %C between 0.8 to 0.18%). Prime quality Wire Rods are sourced as per standards details shown in table 1.

Welding of the mesh happens on a Multi-Spot-Welding Line comprising of the Long & Cross Wire Pitch Con trol & Transport Mechanisms and the Multiple Resistance Welding Guns. Spot Welding is fusing (no foreign filler metal) of the Cross Wire into the Long Wire between Copper Electrodes by Passing Heavy Current at Low Voltage (Approx. 11000 Amps for 5 to 12 mm dia meter welding at about 6-10 Volts) under Heavy Force (Approx. 8kN) for a short duration (Approx. 20 cycles or 0.4 sec). A typical machine is shown in Fig.3.

Table 1: Rel	levant Standard	s Used for	· Weld Wire	e Mesh Fabric

Specification	Title	Parameters	Value
IS:1566	Hard - drawn	UTS	570 MP a Min.
&	Steel Wire Fabric	Yield 0.2% Proof	480 MP a Min.
IS:432 Pt.2	for Concrete	Strength	
	Reinforcement &	Elongation on 8	7.5% Min
	Hard-drawn steel	Times Dia GL	
	wire for concrete	Weld Shear Strength	Min 25% of UTS
	reinforcemen t:		
	Part 2		
BS:4483	Steel fabric for	UTS	1.05 times Yield
&	the		Strength
BS:4482	reinforcement of		500 MPa Min.
	concrete & Steel	Strength	
	wire for the	Total Elongation at	2.5% Min
	reinforcement of		
	concrete	Weld Shear Strength	Min 25% of Yield
	prod u cts		Strength of
			Thicker Dia
ASTM A185	Steel Welded	UTS Grade 80 /	620 MPa Min /
&	Wire Fabric Plain	Grade 60	515 MPa
A82	for	Yield 0.35% Proof	550M Pa Min /
	Reinforcement &	Strength	450 MPa
	Steel Wire, Plain	Reduction in Area	30% Min
	for Concrete	(after Failure)	
	Reinforcement -	Weld Shear Strength	241 MPa in
	Grade 60 &		Thicker Dia
	Grade 80 (80000		
	Psi)		



Fig.3: Automatic Spot Welding Machine for WWF

Pitch Con trol of Long Wires is generally set fixed for one batch and needs resetting for each batch of Long Wire pitch sets. Some New Installations have Robotic type Moving Electrode guns controlled by PLC for quick change over of Long Wire Pitch sets. Pitch Control of Cross Wires is by a Setting Adjustable Mechanical Cam Motion or By Online Variable Stepper / Servo Motor driven Motion.

QUALITY ISSUES

Recommen ded welding is Semi or autom atic multi- spot-welding machines for Resistance welds with no foreign filler metal. The Spot-welding technology works well and reliably with Steels of low carbon (< 0.15 % C) and of homogeneo us Cross-section as in Cold Rolled Ribbed Bars / Cold Drawn Plain Wires. The weld mesh to qualify the shear strength as per IS 4948 for projection welding with the increasing use of advanced high-strength steels, and the emerging trend toward the adoption of simulation resistance welding to reduce weld verification testing and preproduction 6 scrap and labour. The projection welding, it is not possible to weld without expulsion & the problem is controlling the amount of expulsion and obtaining the req uired s trengt h. Stan dardized proced u res are needed for deter mining the weldability of materials for cross wire welding. Hot Rolled TMT bars have higher carbon (typically 0.18-0.30% C) and heterogeneous Cross-section (ou ter h ard Martensite RIM, Transition zone & Inner soft Ferrite / Pearlite Core zone including a spiral fin). Spot welding of TMT bars leads to un reliable and incon sis ten t welds if not done properly. Un reliable welds which may snap in handling are more dangerous than NO WELDS as they lead to loss of Crosssection and design strength.

USES OF WELD MESH

Reinforced weld mes h is u sed in construction, having applications in floor slabs of warehouses as well as residential housing projects with the inclusion in shear walls, to reinforce roadways, walkways and floors. The major advantage of usage of weld mes h is reducing the risk of cracks and deterioration of concrete without the added expense of rebar. Mes h usage cancut down rebar placement times in Slabs & Walls from days to hours. It suse also results in fewer labour costs associated with construction. Welded wire mesh in a variety of industries, from agriculture and horticulture to transportation, mining, and construction.

Reinforcement Bars Diameter like 6, 7, 8, 9, 10 mm of welded wire mesh can make a good in ter n al fr a mework for reinforced concrete structures. Usage of weld mesh provides substantially increased tensile strength to a material that is ot herwise quite vulnerable to cracking under the forces of vibration, twisting, and warping. Also these are used in Road beds, Walkway beds, Concrete foundations, Industrial strength floors and ceilings, Concrete walls, Factory conveyor belts etc. Fig.4 shows weld mesh fabric.

The strengt h a n d flexibility of welded fabric is cr u cial in con s tr u ction a n d reinforcemen t of a rches a n d domes, thereby preven ting the emergence of cracks in the structures. With this construction of arches and domes is easy

otherwise it would have been very cumbersome. Prefab walls are factory assembled based on design requirement and can be installed easily.



Fig.4: Typical Weld Mesh Fabric Ready for Use

REINFORCED CONCRETE PAVEMENT

Continuously Reinforced Concrete Pavement (CRCP) is a type of rigid pavement, employed in highway construction owing to its host of benefits shown in Fig.5. Materials used to inclu de concrete and steel (steel bar, wire fabric) with concrete, den se and low per meability concrete mix is required with a maximum water content ratio of 0.42 to 0.45. Similarly, with steel, which is used in steel bar and fabricated wire mes h forms, specific grades need to be selected based on strength properties. In all, based on the application and end result, the technical specifications for the materials need to be fixed accordingly.



Fig.5: Continuously Reinforced Concrete Pavement

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The pavement forms transverse cracks at close intervals due to the con tin uou s reinforcement, which it self results from the change in concrete volume. Ideally, a thoroughly designed CRCP that's built using superior quality materials can keep the mentioned cracks tightly closed, thereby minimizing water penetration and other similar problems. There are fewer joints and tightly closed transverse cracks, water penetration can be reduced as well. These roads can handle heavier truck loading and volume. While its initial cost is high, it has a longer life cycle, which keeps the overall cost in the long run low.

GRATING

A perfect com bin a tion of s trengt h, low cost, a n d ease of installation m akes welded wire mes h a pop ular choice for grating roads providing ven tilation for subway systems and for covering street side drains as shown in Fig.6.



Fig.6: WWF Used in Grating Beside Road

FENCING

Those looking for a relatively cheap security solution that's tougher than ch ain lin k a n d s till allows visibility will often t u r n to welded wire mes h. Application sites range from lower-security prisons and military installations to private offices and residences. It may even be placed within factories and other in d u s trial buildings as a gu ard material s u rrou n ding heavy machinery as shown in Fig.7.

DECORATIVE PURPOSES

Welded wire mes h is available in multiple colors and coatings, and can in fact make for a visually appealing framework for trellises, flowerbed enclosures, and birdcages among others. Some find it a perfect fit for elevating plants above the ground, or for shelving in garden sheds, closets, and even retail stores.



Fig.7: WWF Used as Security Fencing Purposes

ADVANTAGES OF WWF

The u sage of proper grade of weld mes h in construction will fetch many advant ages. These are improved site efficiency & productivity with reduced reliance on manpower on-site. The chance of improper bending of bars is reduced since bending machines bend the mat as a single unit. Provides the exact size of reinforcement where needed through variable bar size and spacing. The other benefits are as below:

Cost Reduction

Eliminate labour costs on cutting, binding and placing rebars Save cost of binding wire Reduce inventory costs and working capital

Design Optimised

Use any diameter from 2-12mm unlike rebars Optimized designs for reinforcement requirements Reduce overall steel requirement

Smart Execution

Easy tracking to minimize pilferage Easy inspection for structural consultants Perfect spacing through mechanized process Faster Construction and Reduction in Labour

Save Time

A prefabricated solution that reduces slab to slab casting time Ready-to-use materials delivered at site Valuable labour hours saved

FATIGUE PERFORMANCE

Weld wire mesh has been the standard reinforcement for bridge I-girders and inverted-tee girders. Structural mem bers fail due to fatigue when cracking develops under repetitive loads that are less than their static load capacity. T he process s t a rt s with t he initiation of cracking, followed by propagation of cracking, in which micro-cracking grad ually takes place in t he concrete or cracking grows in a s teel element. Slow crack growt h is followed by a brief period of quick growt h, which leads to the third stage: fr act u re. WWR is more desirable t h an defor med bars for fa tigu e application s because after first wire fracture, alternate load paths are available through t he fabric and multiple fr act u res h ave to occu r before t he perfor m a nce of the concrete panel is severely affected.

CORROSION ISSUE

The p H of h ardened concrete is alkaline and is generally in the r ange of 12.6 to 13.5. Carbon ation will result in red uction of p H of concrete resulting in rupture of passivating layer around the embedded reinforcement which ot herwise protects it from corrosion. Weld mes h wire / bars u sed a re cold drawn, hot rolled, cold twisted and quenched & tempered used for construction. The microstructures are different from pearlite ferrite (cold drawn) to tem pered marten site (QST Rebars) and steels are having residual stresses (Tor). It is expected that there will be variation in polarization beh avior and corrosion r a tes of all t hese s teel wit h differen t microstr u ct u res. It is reported t h a t corrosion r a te increases in t he following seq u ence: pearlitic to marten sitic to tem pered marten sitic steels when pH value drops to a greater extend. Though the corrosion starts and continues with the creation of galva nic cell between cat hodic carbide a n d a nodic ferrite p h ases, corrosion mechanism differs for the steels with microstructures, attributing to the size, shape, and distribution of galvanic couple.

CONCLUSION

Welded wire fabric is used as reinforcement to add to the strength of slabs and ensure a stronger, more stable overall construction. There are a variety of advantages associated with the use of welded wire fabric or reinforcing bars in a slab. This article has looked at some applications of weld wire mesh using cross wire welding and are also made from hot rolled steel, cold drawn and TMT bars in stead of the st an dard In ter n ation al Specs accepted practice of using cold rolled ribbed bars, cold drawn plain wires. Many designers are reluctant to use weld wire mesh as an alternative to mild steel reinforcing bars due to the unavailability of fatigue design guida nce. Corrosion st u dies are also im port to evalu ate the durability of concrete with respect of steel types having different microstructures. Both CTD and TMT bars of high strength steel have a not her shortcoming to contend with the effect of stresses on corrosion is reflected more distinctly in the mech anical ch ar acteristics of the reinforcement, specially of high-strength steels with low ductility.

ACKNOWLEDGEMENT

Author is thankful to Weld Mesh Manufacturers Association (WMA) for providing an opportunity to work with the weld mesh wire fabric product usage in construction segment. WMA has been at the forefront in developing products that are equipped with best-in-class features pertaining to durability, cost-effectiveness without any compromise on the quality.

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INNOVATIVE USAGE OF STEEL HOLLOW SECTIONS IN STEEL-BASED CONSTRUCTION

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ABSTRACT

Steel hollow sections are proving to be the most versatile and efficient for m of structural steel for construction and mechanical applications. Many of the iconic and most impressive s tructures in the world would not have been possible without use of hollow sections.

Tata Structura was la unched in 2005 and is currently the leading steel hollow section brand in project construction in India. Tata Structura has been used in more than 40 airports, 20 stadiums, 7 metro projects and many more iconic projects across India. Tata Structura YST 355 was la unched in 2015 and was the first brand to la unch YST 355 grade steel hollow section in India.

In this report, we are covering two topics regarding innovative u sage of s teel hollow section in steel-based construction as part of our initiatives from Tata Structura:

- a) Concrete filled tubes (CFT)
- b) Concept of Diagrid structures

INTRODUCTION

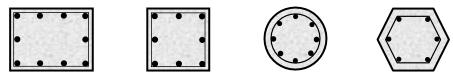
Concrete filled steel tubular members, comprising a hollow steel tube infilled with concrete, have been used in many structural applications, especially for column s in high rise b uildings a n d bridge piers. The ot her applications include structural uses in infrastructure, industrial buildings, offshore oil and gas installations and retaining or supporting structures.

Concrete-Filled Steel Tubes (CFTs) are composite members consisting of a steel tube in-filled with concrete with or without reinforcement (Fig. 1). In current international practice, CFT columns are used in the primary lateral resista nce system s of bot h braced and un braced building structures. There exist application s in J apa n and E u rope where CFTs are also u sed as bridge piers. Moreover, CFTs may be utilized for retrofitting purposes for strengthening concrete columns in earthquake zones.

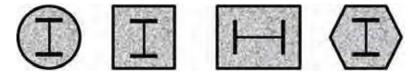
The concrete core adds com pressive s trengt h a n d s tiffness to t he t u b ular colum n which red u ces possible for inward local b u ckling. The s teel t u be acts as longit u din al a n d la teral reinforcement for t he concrete core helping it to resist ben ding moment, s hear force and twisting moment which provides confinement for t he concrete. Since t he benefit of t hese composite action of two such materials, CFT columns provide better seismic resistant structural properties such as rise in ductility, increase in strength and enormous energy absorption capacity.



Concrete filled tubes without reinforcement



Concrete filled tube with reinforcement



Concrete filled tube with an encased steel section inside

Fig.1: Concrete Filled Tubes with or without Reinforcement

ADVANTAGES OF CONCRETE-FILLED STEEL TUBES

The CFT structural member has a number of distinct advantages over an equivalent steel, reinforced concrete, or steel-reinforced concrete member.

1. The Concrete Filled Steel Tubular (CFST) column offers numerou s s tructur al benefits, including high strength, fire resistance and higher energy absorption.

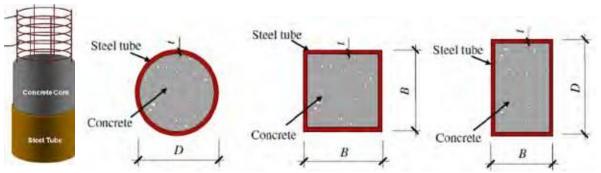


Fig.2: Concrete Filled Steel Tubular Column

2. The orien t a tion of t he s teel and concrete in t he cross section optimizes the strength and stiffness of the section. The steel lies at the outer perimeter where it performs most effectively in tension and in resisting bending moment.

- 3. Also, the stiffness of the CFT is greatly enhanced because the s teel, which h as a much greater mod ulu s of elasticity t h a n t he concrete, is situated fart hest from the centroid, where it makes t he greatest contribution to the moment of inertia.
- 4. The concrete for m s a n ideal core to with s t a n d t he com pressive loading in typical application s, and it delays and often prevents local b uckling of the steel, particularly in rectangular CFTs.
- 5. Addition ally, it has been shown that the steel tube confines t he concrete core, which increases the compressive strength for circ ular CFTs, and the ductility for rectangular CFTs. Therefore, it is most advantageous to use CFTs for the columns subjected to the large compressive loading.
- 6. In contrast to reinforced concrete columns with tran sverse reinforcement, the steel tube also prevents spalling of the concrete and minimizes congestion of reinforcement in the connection region, particularly for seis mic design.

Recent applications have also introduced the use of high strength concrete combined with high strength thin-walled steel tubes with much success. When high strength concrete and thin-walled steel tubes are used together, the more brittle nature of high strength concrete is partially mitigated by the confinement from the steel tube, and local buckling of the thin steel tube is delayed by the support offered by the concrete. Progress in concrete technology has made it possible to utilize concrete strengths over 100 MPa in CFT beam-columns.

In addition to t he above adva n t ages, we can see several ot her economic benefits branching from the use of CFTs.

The tube serves as for mwork in construction, which decreases labor and material costs. In moderate- to high-rise construction, the building can ascend more quickly than a comparable reinforced concrete structure since the steelwork can precede the concrete by several stories. The cost of the mem ber itself is much less than steel and roughly equivalent to reinforced concrete on a strength per dollar basis for low to medium strength concrete.

When com pared to steel moment resisting frames, in unbraced CFT frames, the amount of savings in steel tends to grow as the number stories increases.

On the other hand, relatively simple beam-to-column connection details can be utilized for rectangular CFT mem bers. This also results in savings for the total cost of the structure and facilit ates the design process.

In addition, the steel tube and concrete act toget her to provide natural reinforcement for the panel zone, which reduces the material and labor costs of the connections. With the use of highs trengt h concrete, CFTs a re s tronger t h an conven tion al reinforced concrete columns for equivalent cross-sectional area.

In high-strengt h application s, s m aller colum n sizes m ay be u sed, increasing the a mount of u sable floor space in office buildings. The s m aller and lighter framework places less of a load on the foundation, cutting costs again. These advantages have secured an expanding role for this versatile structural element in moder n construction.

STRUCTURAL BENEFITS OF CONCRETE-FILLED STEEL TUBES

The concrete core adds stiffness and compressive strength (Fig. 3) to the t u b ular colum n a n d red u ces t he poten tial for inward local b u ckling. Conversely, the steel tube acts as longitudinal and lateral reinforcement for the concrete core helping it to resist ten sion, ben ding moment and shear and providing confinement for the concrete.

Due to the benefit of composite action of the two materials, the CFT columns provide excellent seismic event resistant structural properties such as high strength, high ductility and large energy absorption capacity

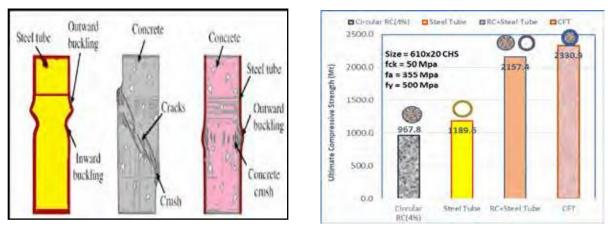


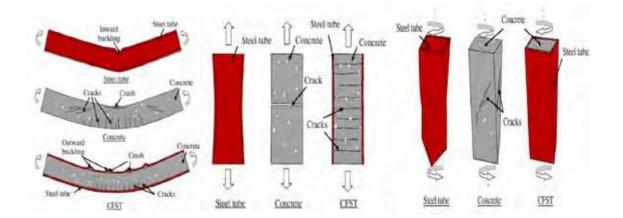
Fig.3: Axial Compressive Strength for Different Stub Columns

The compressive strength of the CFT column is seemed to be higher than the arithmetic sum of the strengths of RC column (4% reinforcement) and steel tu be withou tany fill, due to the effect of confinement of concrete by the ou ter skin of steel tu be. The effect of confinement is more in case of a circ ular section in-filled with concrete than a ny sh aped section filled with concrete. The structural benefits of CFT in case of other structural elements can be seen below:

DESIGN PERFORMANCE ANALYSIS OF CFT COLUMNS

- a) Com parative a n alysis of Colum n s wit h or wit hou t fill of concrete of different grades is shown in Fig. 4. The com pressive s trengt h of colum n s increases by almost twice in case of la rge dia. HS filled with higher grade of concrete like M50 or M60.
- b) Comparative a n alysis of RCC Colum n s vers u s CFT colum n s with same cross- sectional areas is shown in Fig.5 and Fig.6.

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	Comp	ression Cap		
Hollow Section	Without Fill	Concrete Grade	With Fill	
		M20	1636	
CHS 610x20	1189.6	M30	1798	
	1189.0	M40	1958	EUROCODE 4
		M50	2119	ANSI/AISC 360-16
		M20	1621	GB 51249-2017
SHS 500x500x20	1221.6	M30	1755	ACI 318
SHS 500X500X20	1221.6	M40	1887	
		M50	2020	✓ IS 11384 (Under Draft)

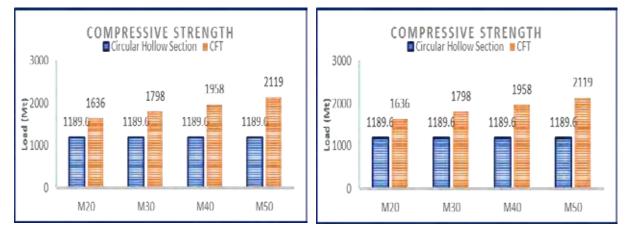


Fig.4: Advantages of CFT in Different Structural Elements

	Compre	ssion Capad	city (Mt)	COLUMNS OF SAME CROSS					
	Concrete Grade	CFT	Circular RC(4%)	4000		CTIONAL CFT ■ Circul		2119	
CHS 600x20	M20	1635.8	625.8	2000	1635.8	1798		967.8	
	M30	1798	739.8		625.8	739.8	853.8	967.8	
	M40	1958.6	853.8	0					
	M50	2119	967.8		M20	M30	M40	M50	

Fig.5: Circular RC Columns (4% reinforcencement) Versus Circular CFT Columns

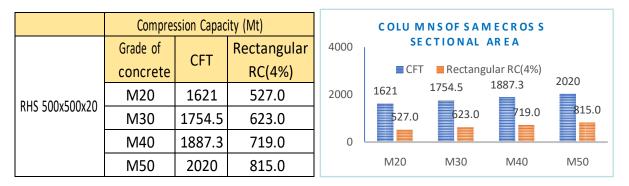


Fig.6: Square RC columns (4% reinforcencement) Versus square CFT Columns

ADVANTAGES OF CFT IN MULTI-STOREY BUILDINGS

- Delayed local buckling & Strength enhancement due to confining effect
- □ Reduction in drying and creep shrinkage
- □ Saving of manpower, constructional cost, and time
- □ Increased usable floor area due to reduced column size
- □ Improvement in fire resistance performance
- □ Safer and more reliable in seis mic region
- **\Box** Reduction in overall Construction Time by $1/3^{rd.}$
- □ Reduction In steel Consumption by 15 -20%
- □ Better fire resistance of up to 60 minutes
- □ Reduction in Space of the RCC Column Size by 30 40%, more usable plinth area
- □ Overall Cost Saving in the tune of 10 -20%

KEY CFT PROJECTS IN INDIA

L&T Business Towers and Business Park, Mumbai

Box section used:

1200 mt of 1100x800x16 Prim ary application for columns

Technology Adopted:

Concrete filled tubes Usage of CFT columns with no reinforcement enabled the construction of 3 floors simultaneously

Total construction time = 27 months

Slab cycle time was reduced to 7 days and overall time savings of 3.6 months was achieved



Project was completed successfully by L&T Reality

Fig.7: Some Major CFT Projects Outside India

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LIMITATIONS OF CONCRETE-FILLED STEEL TUBES

- 1. A prim a ry deterrent to widespread use of CFTs is the limited knowledge regarding their behavior.
- 2 . A num ber of factors com plicate the an alysis and design of concrete-filled steel tubes. A CFT mem ber contains two materials with different stress-strain curves and distinctly different behavior. The in teraction of the two materials poses a difficult problem in the deter mination of com bined properties such as moment of inertia and modulus of elasticity.
- 3. The failu re mech a nis m depen ds la rgely on t he s h ape, lengt h, dia meter, steel t u be t hick ness, and concrete and steel strengt h s. Para meters s u ch as bon d, concrete confinemen t, resid u al s tresses, creep, s h rin kage, and type of loading also h ave an effect on t he CFT's beh avior.
- 4 . Axially loaded columns and, in more recent years, CFT beam-column s and connections, have been studied worldwide and to some exten tmany of the issues have been reconciled for these types of mem bers. However, researchers are still studying topics such as the effect of bond, confinement, local buckling, scale effect, and fire on CFT mem ber strengt h, load transfer mech anisms and economical detailing strategies at beam-to-CFT column connections, a nd categorization of response in CFTs and their connections at all levels of loading so as to facilitate the development of performance-based seismic design provisions.
- 5. It should also be noted that, despite a recent increase in the num ber of full-scale experiments, the majority of the tests to date have been

conducted on relatively small specimens, often 6 inches in diameter or s maller. This is d u e to the load limits of the testing apparat u s and the need to r u n the tests economically. Whet her these results can be acc u r a tely extrapolated to the typically la rger columns u sed in practice remains a pertinent and debatable question.

DIAGRID STRUCTURES

The basic idea for developing a diagridsystem is to elimin a te vertical columns. Vertical columnscarry only gravity loads and incapable of providing la teral stability. A tall building should resist both gravity loads and lateral loads (due to wind, earthquake, etc.). Diagrid system provides this facility. This structural system resists both gravity and lateral loads, by the action of axial forces in an effective manner. Diagrid is an exterior structural system consisting of only inclined columns on the façade. The Concept of diagrid evolved from the braced tubular structure system s. The skin of the building is a truss network of hollow section s with nodes that are welded during assembly. Steel floor beams are spanned between the perip heral nodes and cen tral ring bea mandt hese floor beam s support the com posite floor slabs. The core that hou ses the services has columns of reinforced concrete with optimal and varying thickness of structural steel usage.

- □ Absence of vertical members in the perimeter of diagrid system
- Diagonals acting as both inclined columns and bracing elements
- □ Shear and overturning moment developed are resisted by axial action of diagonal members

Advantages of Diagrid System

- Maximum exploitation of the structural material
- Aesthetically dominant and expressive
- 20% reduction in steel as compared to braced frame
- Good day lighting due to dearth of interior columns
- Sustainability, Energy efficiency & Low environmental cost

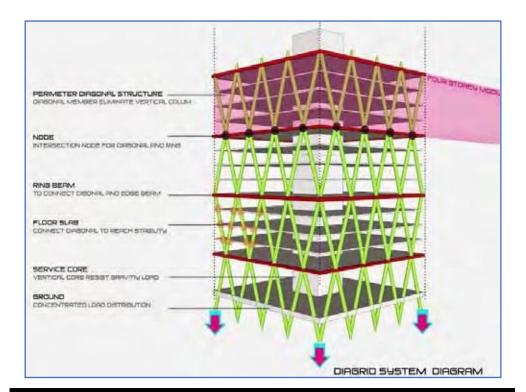
Structural Benefits in Dia-grid Framework

 Good respon se to inten se la teral press u re in t all commercial b uildings Useful for bot h gravity and la teral loads for la rge span and high-rise buildings

Key CFT Projects in India

a) I-Lab Building, Hyderabad (Designed by Construction Catalyser)

This unique oval dome shaped (55 m x 23 m x 21 m) design is demon strated by an exclu sive dia-grid concept used effectively to provide good visual lightness and barrier-free usable office spaces inside. The self-supporting structure with minimal vertical supports imparts the building an innovative look and reduces low life cycle costs further. This five-storied prefabricated light weight structure took eight months for construction.



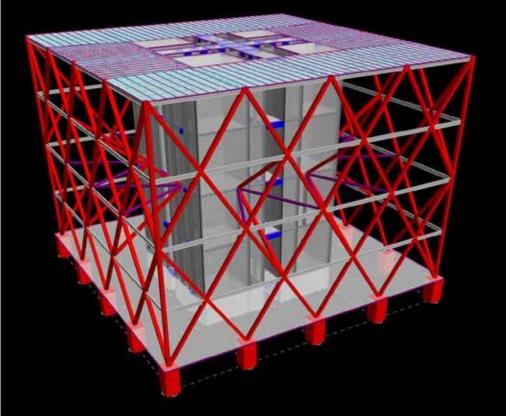
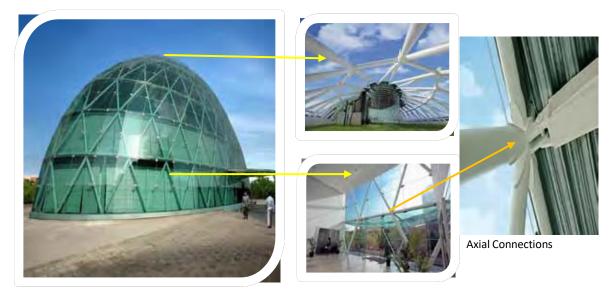


Fig.8: Modelling of a Diagrid Structure

The i-Lab building has become an icon in its class – and it owes this status to the unique approach towards the merit of the structure and architectural manifestation.



I-Lab building, Hyderabad

Roof & Façade view

b) Elevate Interior building, Bangalore (Designed by Op us Architect, Bangalore)

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LIMITATIONS / CONSTRAINTS IN THE DIAGRID FRAMEWORK KNOW-HOW:

- Unavailability of skilled workers
- Limited exploration in the field of Diagrid construction techniques
- Difficulty in erection of Nodes
- Complex engineering in design and fabrication of Joints
- Dependency of number of storeys on the primary module height

CONCLUSION

Structural Hollow Section sare the most efficient of all structural steel section s in resisting com pression. Tata Structura hollow section s have a high strength to weight ratio and produce slender attractive lines that make them a natural choice for building structures. These hollow sections can achieve a constant external dimension for all weights of a given size, which enables them to achieve standardisation of architectural and structural details throughout the full height of the building if required. Concrete-filled s teel t u be (CFT) colum n s com bine t he adva n t ages of d u ctility, generally associated with steel structures, with the stiffness of a concrete structural system. While many advantages exist, the use of CFTs in building construction has been limited, in part, to a lack of construction experience, a lack of understanding of the design provision s and the complexity of connection detailing. The new-age structural material from Tata Steel has opened up a world of possibilities for all these innovative technologies. The presence of higher grade like YST 355 and large dia. sections (up to 600 NB in CHS, 400x 400 in SHS and 400x 200 in RHS) has provided a support to designer to think beyond the expected.

Diagrid - Diagon alised grid struct u res is one of the emerging innovative concepts to design tall buildings. Diagrid - a word for med by com bin ation of "diagon al" and "grid". Diagrid structures act like free standing cantilevers and resist both, gravity, and lateral loads, by the action of axial forces in an effective manner. It is observed that, in diagrid 33 % less steel is required than conventional building. Also, architecturally diagrid structures give more aest hetic than convention al building. The steel hollow sections from Tata Structura have en abled designers, architects, and engineers to add wings to their im agin ation. They are now able to explore new ways and experiment more with innovative design s to boost aest hetics, strengt h, and durability of their creations with the help of Tata Structura hollow sections. With Tata Structura available grade & hollow sections, this innovative structural framework will also get a boost in the emerging trend of construction.

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A JOURNEY INTO THE WORLD OF CORROSION

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INTRODUCTION

The word corrode is derived from the Latin word "corrodere" which means "to gn aw to pieces" Corrosion can be defined as a chemical or electrochemical reaction between a material, usually a metal/alloy, and its environment that prod u ces a deterioration of the material and its properties. Often corrosion results in the damage to the usage of the material considered inspite of the best design, fabrication and main ten ance. In this article, a brief has been provided on the chemistry of corrosion, factors affecting the rate of corrosion, major types of corrosion encountered, effects of corrosion on the steel structure and major accidents reported, corrosion prevention and management. A synopsis on the case study of corrosion in a spray drying tower of a detergent manufacturing plant is also included.

CHEMISTRY OF CORROSION

Corrosion is a n electrochemical process, which in t he presence of moist air, degrades and even tu ally leads to loss of surface material. However t his is a time depen den t process, i.e. t he longer a com ponen t is exposed to corrosive environmen t, t he more it corrodes. High h umidity co u pled with t he presence corrosive chemicals in dust or vapor form, high a mbient tem perat ure and in adequate air circulation are some of the main reasons for corrosion.

Stru ct u r al s teel is an alloy m ade u p of m ainly iron a n d a sm all percen t age of carbon; t he fin al prod u ct after t his degradation is called r u st. This reaction is often called a n oxidation reaction since t here is t he for m ation of respective oxides at the end of the process.

Initial attack occurs at anodic areas (Fig. 1) on the surface, where ferrous ions go into solution. Electrons are released from the anode and move through the metallic structure to the adjacent cathodic sites on the surface, where they com bine with oxygen and water to form hydroxyl ions. These react with the ferrous ions from the anode to prod uce ferrous shydroxide, which is further oxidized to prod uce hydrated ferric oxide (i.e. red rust.) The sum of these reactions can be represented by the following equation:

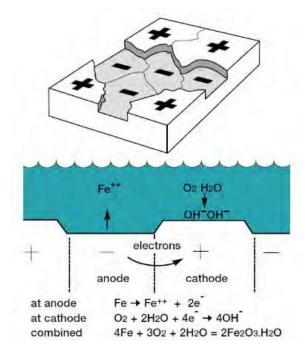


Fig.1: Chemical Reactions of Corrosion Process

Fe	$+ 3O_2$	$+ 2H_2O$	=	$2Fe_2O_3H_2O$
(Steel)	+ (Oxygen)	+ (Water)	=	Hydrated ferric oxide (Rust)

The corrosion process req uires the simulta neo us presence of water and oxygen. In the absence of either, corrosion does not occur. The process is facilitated by the presence of dust and chemicals.

FACTORS AFFECTING THE RATE OF CORROSION

The electrolyte is u su ally water. The flow of electron s is from a node to cat hode. As negatively ch arged electron s leave the a node, positively ch arged ion s of the a node metal are released in to the electrolyte. These ion s can react with ot her materials to form corrosion products called "rust". Due to this, the anode is damaged and the cat hode is undamaged. Since, there is presence of a metal (steel), electrolyte (moist environment such as water) and current flow through

t his electrolyte from a node to cat hode (galva nic couple), the corrosion process can be compared to a simple "corrosion cell." An oxygen cell is a type of corrosion cell in which oxygen concentrations in the electrolyte determine the a node and cat hode locations. Locations where the electrolyte oxygen concentration is low (such as stagnant standing water) are anodic and prone to corrosion. Metals at point of low ion concentration corrode. In some cases, certain bacteria can also affect the rate of corrosion because their metabolic processes can alter the oxygen and metal ion concentrations in the electrolyte. Among many other factors, corrosion can also be affected by environmental effects which include temperature and humidity. High temperature increases the rate of corrosion. The amount of moist ure available is very crucial to the rate of corrosion because water serves as an electrolyte. In regions where water is scarce, corrosion rate is slow compared to regions with above-average precipitation. Exposure is important in assessing corrosion on a single structure. Areas exposed to wind or sunthat can dry quickly are less prone to corrosion than sheltered areas where water can remain in contact with the metalwork.

Salt spray from breaking waves and on shore winds significantly accelerates the corrosion of steel structures in marine environments. The ocean salts, which are primarily sodium chloride but include chlorides of other metals such as potassium or magnesium, acc umulate on the metal surfaces and accelerate the electrochemical reaction sthatcauserusting and ot her forms of corrosion. The combination of salt accumulation on the surface and the high humidity common to many coastal areas significantly accelerates the corrosion rate of steel. The longer a surface remains damp during normal daily fluctuations in humidity, the higher the corrosion rate. On shore winds carry both salt and moist ure inland. Therefore, corrosion rates along shorelines with predomin ately offshore winds.

MAJOR TYPES OF CORROSION

Unifor m Corrosion Galvanic or Bimetallic Corrosion Crevice Corrosion Pitting Corrosion Stress Concentration Cracking

Uniform Corrosion

Unifor m corrosion is the most common type and is characterized by attacks over the entire surface area of the metal exposed to a corroding agent. This type of corrosion is typically caused by chemical or electrochemical reactions that cause the metal to be consumed while for ming oxides or ot her com pounds over large visible areas.



a. <u>Galvanic/Bimetallic Corrosion:</u>

Bimetallic corrosion, also k nown as galva nic corrosion, is the corrosion that occurs when two dissimilar metals are directly or in directly in contact with each ot her. Visually, this type of corrosion is characterized by the accelerated deterioration of one metal, while the other remains less affected.

Bimetallic corrosion is a purely electrochemical reaction driven by t he difference in electrode poten tials between t he two metals. When exposed to an electrolyte, the two metals for m a type of cell known as a bimetallic couple, where one metal acts as the anode and the ot her as the cat hode. The movement of electrons from the anode to the cat hode initiates an oxidation reaction at the anode that causes it to be dissolved, i.e., corrode.

Metals that are further from each other in the "Galva nic Series" have the highest r a te of corrosion when com bined. By k nowing the relationships of the metals in the series, galvanic compatibility can be determined, preventing the possible harmful effects of galvanic corrosion.





Galvanic corrosion due to different anodic index between the bolt and a plate

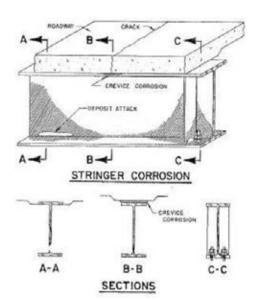
ANODE			
ANODE	1. Magnesium	9. Nickel (Active)	17. Stainless Steel 304 (Passive)
	2. Zinc	10. Inconel 600 (Active)	18. Stainless Steel 316 (Passive)
	3. Aluminium alloys	11. Brasses	19. Titanium
	4. Aluminium	12. Copper	20. Haste alloy C276
	5. Mild Steel	13. Bronzes	21. Silver
	6. Cast Iron	14. Nickel (passive)	22. Graphite
	7. Stainless Steel 304 (Active)	15. Inconel 600 (passive)	23. Gold
CATHODE	8. Stainless Steel 316 (Active)	16. Monel 400	24. Platinum

Galvanic series of Metals (Anode End to Cathode End)

b. <u>Crevice Corrosion:</u>

Crevice corrosion is a highly penetrative type of localized corrosion that occurs in or directly adjacent to gaps or crevices on the surface of a metal. These crevices can be the result of a connection between two surfaces (metal to metal or metal to nonmetal), or by an accumulation of deposits (dirt, mu d, biofouling, etc.). This type of corrosion is characterized by deterioration in the area of the crevice.

One of the main criteria for the development of crevice corrosion is the presence of constant water within the crevice. This lack of fluid movement gives rise to the depletion of dissolved oxygen and an abundance of positive ions in the crevice. This leads to a series of electrochemical reactions that alters the composition of the fluid and makes it acidic in nature. The acidic liquid in the crevice breaks down the metal's passive layer and renders it vulnerable to corrosion attack.





Crevice corrosion in beams

c. <u>Pitting Corrosion:</u>

Pitting corrosion, also known as pitting, is another localized form of corrosion that occurs on metal surfaces. Pitting typically manifests itself as small diameter cavities or holes on the object's surface while the rem ain der of the metallic surface rem ain s less affected. This for m of corrosion is also highly penetrative and is considered to be one of the most dangerous types of corrosion because it is difficult to predict and has a tendency to cause sudden and catastrop hic failures.

Pitting usually originates on areas of the metal surface where incon sistencies in the protective passive film exist. These inconsistencies may be due to film damage, poor coating application or foreign deposits on the metal surface. Areas where passivity has been reduced or lost now become the anode while the surrounding region s act as the cat hode. In the presence of moist ure, the anode and cathode form a corrosion cell where the anode (i.e., the areas unprotected by the passive film) corrodes. Beca use the corrosion is confined to a localized area, pitting ten ds to penetrate the thick ness of the material. The formation of pits is often a precursor to other forms of localized failures such as metal fatigue and stress corrosion cracking (SCC).



Pitting corrosion of steel columns in a detergent manufacturing plant due to the presence of salt and active matter.



Pitting corrosion of steel beam in a salt manufacturing plant

d. <u>Stress Corrosion</u>

Stress corrosion cracking (SCC) is a form of corrosion marked by the formation of fine cracks on specific areas on the metal surface while

t he metal rem ain s less affected over most of it s s u rface a rea. Often noticed initially as s u rface cracks, they progressively join each ot her in a reas with likelihood of locked-in resid u al / ten sile s tresses d u ring t he process of fabrication – welding, heat treat men t and cold defor m a tion s. SCC is con sidered to be a n in sidiou s for m of corrosion beca u se t he damage is sometimes not immediately detected d uring in spections, which suddenly aggravates to cause rapid loss of strength and consequent failure.

Effects of corrosion on steel struct ure and major accidents reported due to corrosion:

The corrosive reaction changes the microstructure of the steel on its surface, thus making it brittle and flaky. Slowly it loses its mechanical strength and elasticity. Thus, the useful life of steel structures and other application s are severely curt ailed. Non – unifor m corrosion s u ch as pitting, crevice, galvanic and SSC are dangerous forms of corrosion that may lead to sudden and catastrophic failure.

Some of the major failure incidents are listed below:

NAME OF ACCIDENTS	YEAR	PLACE	REASON AND DAMAGE
Silver Bridge Collapse	1967	Ohio, USA	The U.S. highway 35 bridge in between Point Pleasa nt, West Virginia a nd Ka na uga, Ohio fall down into the Ohio river. Stress corrosion cracking a nd corrosion fa tigu e was respon sible for this collapse. This accident claimed over 46 lives.
Bhopal Acciden t	1984	Bhopal, In dia	Methylisocyanate (MIC) storage tank leaked due to corroded pipelines, valves, and other safety equip ment at Union Carbide In dia Ltd. cau sed the release of MIC and other chemicals into the surrounding area. Almost 3000 people killed, and over 500,000 people were injured.

Rupture of a High- Pressure Vessel	2009	Illinois, USA	Stress Corrosion Cracking of t he walls of a press u re vessel ca u ses Nihon Dem pa Kogyo (NDK) Com pa ny explosion.
Swimming Pool Roof Collapse	1985	Uster, Switzerla n d	After 13 years of use, the concrete roof supported by s t ainless s teel bea m s collapsed d u e to s tress corrosion cracking.

Corrosion Prevention and Management:

Corrosion is the biggest single cause of plant and equip ment breakdown in the industry. However, corrosion is often not uniform and it is estimated that only 35 % failure of a chemical plant are due to general / unifor m corrosion. The most common cause of corrosion failure have been discussed above. Most of these can either be controlled or eliminated if proper measures are adopted.

Some of the meas u res a re:

- a. Material Selection
- b. Anodic and cathodic protection
- c. Engineering design of components
- d. Use of special coatings and ot her sop histicated s u rface protective applications

a. Material Selection:

Since the materials available for fabrication of equipment and structures are large, the factors, such as, resistance to corrosion in a given environment, peculiar tendency of materials to specific types of corrosion, and special treatments should be coordinated with the functional parameters. Strength, fabricability, ease of production, appearance, availability and cost should be considered. It may be necessary to compromise and sacrifice some advantageous properties to satisfy corrosion requirement ts and vice-versa. Using fully corrosion resistant material is not always the correct choice; a balance between the first cost and the cost of subsequent maintenance should be found over the full estimated life of the desired utility.

Certain combinations of metal and compatibility are a natural choice. These are:

Materials of Construction	Ideally used in				
Aluminium	non-staining atmospheric exposure				
Chromium containing alloys	oxidizing solutions				
Copper and alloys	reducing and non-oxidizing environments				
Hastealloys	hot hydrochloric acid				
Lead	dilute sulphuric acid				
Monel	hydrofluoric acid				
Nickel and alloys	caustic, reducing and non-oxidizing environments				
Steel	concentrated sulphuric acid				
Tin	distilled water				
Titanium	hot strong oxidizing solutions				
Tantalum	ultimate resistance				

b. Anodic and cathodic protection:

Dissimilar metals in in tim ate contact or connected by a conductive path should be used only when the functional design or other important consideration render them unavoidable. Wherever possible, select materials in contact, close toget her in the EMF series. Exposed a rea of less noble metals should be kept large, relative to more noble metals. If joining of non-com patible metals is unavoidable, dielectric separation is imperative. This can be provided in many ways as for in stance in sulating, gaskets and protective coatings. Figures 5.A and 5.B show ways in which corrosion is prevented in such cases. In Fig. 5.A apart from the use of dielectric insulation separating the aluminium footing and steel pad, a zinc ch rom ate primer may be used to cover surfaces in contact. In Fig. 5.B in stead of using a copper coil, a nickel plated copper coil is preferable.

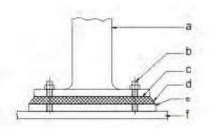


Fig. 5.A Dielectric Separation of Metals: (a) Aluminium Footing, (b) Stainless Steel Stud, (c) Dielectric Insulation, (d) Sealant, (e) Steel Pad, (f) Steel Plate

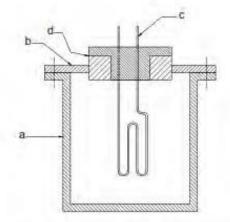


Fig. 5.B Dielectric Separation of Metals: (a) Galvanised Steel Tank, (b) Cover, (c) Nickel Plated Copper Coll, (d) Insulation

c. Engineering design of components:

The main consider a tion s which will help to prevent corrosion a re essentially based on an appropriate shape of the component, concentration of stresses due to loading, the surface conditions and precautions in fabrication.

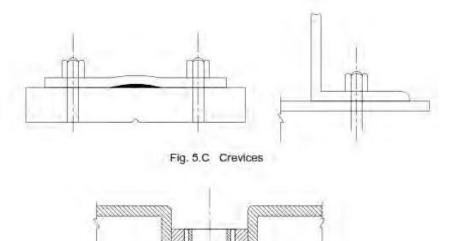
Each component will have to be designed to avoid concentration cells and crevice corrosion. Crevices can be avoided by using welded joints in preference to bolted or riveted joints. Un avoidable crevices as shown in Fig. 5.C may be caulked or sealed.

Whenever possible, horizontal surfaces exposed to the atmosphere should be avoided, since these tend to hold moist ure and dirt. Dis hend heads for vessels are preferable to flat heads. Opport unities for the collection of concentrated solutions and corrosive materials at inaccessible positions in liquid-carrying equipment must be minimized. For example, provision is required to be made for the complete drain age in t an ks and vessels (Fig. 5.D). Inlet or ou tlet nozzles must not project into the vessels and tanks.

Crevices, s h arp cor ners a n d projection s a re ca u ses for corrosionerosion a tt ack. Uneven s tress distribu tion s hould be avoided in corrosive conditions. Localized stresses in any metal component in ten sify corrosion, viz., drilling of bolt holes sets u p u nequ al s tress distribution.

The a rea s u rrou n ding t he hole becomes a nodic a n d is t h u s s u sceptible to attack in a corrosive environment.

To relieve s tresses in fabrication s u ch as welding, m achining, forging, etc., s tress relief through heat treat ment should be specified. Rough s u rfaces a re more s u sceptible to corrosion t h a n s moot h s u rfaces. Likewise, projection s a n d s h arp cor ners a re prone to corrosion-erosion failu res. All fabrication marks, rough joints, weld heads and pipe b u rrs should be removed. Welded joints should be ground flushed.



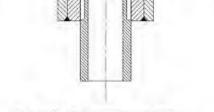


Fig. 5.D Drainage from A Tank

d. <u>Use of special coatings and other sophisticated surface</u> protective applications:

Protective met hods com prise of providing separation of s u f aces from environment, cat hodic protection or anodic polarization. These met hods can be used in divid u ally or in various combinations. Separation of materials from environment, provided by application of metallic coatings, by join ting, coating with plastics or cera mics, by lining, sealing, enveloping, and insulation and by application of tem porary protectives (oils, greases, removable plastics, etc.) involves primarily a change in the surface composition and this change is brough t about by addition s of different materials in the form of an ou ter skin. Most of these processes involve a dimen sion al change and a weight change.

Cat hodic protection is the application of a direct current from an a uxiliary anode to preven tor retard the corrosion of metal which has been made the cathode in the corroding media. For example, by installing an anode near a metal component of the structure, the areas of the metal (anodic or cathodic) within the range of the electrolyte all become cat hodic. This current, when properly applied, opposes the corrosion current from the surface of the protected metal and will minimize corrosion.

Electrolytic anodes are used with external power source, and may be eit her sacrificial or non-sacrificial. Sacrificial or expendable anodes may be iron, steel or aluminium. Aluminium is preferred due to its light weight, uniform corrosion rate and white or colorless corrosionprod ucts. Non-sacrificial anodes may be platin um, high-silicon iron, grap hite and carbon. These are more expensive but last longer. Cathodic protection is used to protect pipelines, tanks, heat exchangers, etc.

Inhibitors are also used for control of corrosion. This is in the form of a chemical, which, when added in small amounts to the corrosive medium, markedly reduces the rate of chemical attack. They are believed to form and main tain upon the metallic surface a protective film, which decreases the corrosion current and renders the environment non-reactive. Inhibitors can control either the anodic or cat hodic corrosion reaction and are, therefore, k nown as either anodic or cat hodic inhibitors. Anodic inhibitors include chromate, silicate, and nitric salt of sodium and potassium. Glassy p hosp h ates and many organic compounds function as cathodic inhibitors. Cathodic and anodic inhibitors acting together are more effective than either of them

separately. In addition to above, protective coatings and linings are u sed for vessels, piping (pips, ben ds and valves) and s torage t an ks, as protective means.

Protective Coatings:

Quite often limitations areim posed by cost and fabrication requirements on the choice of the most desirable material for resisting corrosion. Therefore, a protective coating on a less resistant metal or alloy represents a practical compromise. There are three general categories of coatings: metallic, inorganic and organic. A coating should be applied only on a clean surface. The presence of grease, oil, dirt or scale adversely affects the adherence, continuity and durability of coatings. The surface preparation is one of the most im portant acts for the durability of coatings.

Metallic Coatings:

Ma ny differen t techniq u es a re practiced commercially for applying metallic coatings. These can be classified as a nodic or cat hodic. The a nodic processes will protect t he coated metal through their preferential corrosion, whereas the noble metal coatings are mainly u sed for their s u perior corrosion resistance properties. The most common met hods a re hot-dipping, cement a tion, mech a nical cladding, electroplating, metal spraying and con den sation of metal vapors. Carbon s teels a re some of the most commonly coated metals.

An important met hod of metallic coating is cladding, which is of in terest in the pressu revessel in dustry. The cladding metals in the form of thin plates are bonded to the backing steel plates either by hot rolling or by explosion cladding. The backing plate is ordin a rily of plain carbon steel, but for special applications low alloy steels can also be used. The cladding metals are stainless steels, mainly austenitic types, nickel, monel, copper and cupro-nickel.

Cladded plates a re economical, since t he corrosion resista nce of special cladding metals is obtained, by the use of only a thin layer of the material. Cladded plates can be fabricated by cutting, shearing, welding, etc.

Inorganic Coatings:

Commercial inorganic coatings for protection of metals fall into two general categories, namely, chemical or electrochemical surface conversion treatments and vitreous enamels. Those in the first group often do not constitute the final protective layer but serve as an undercoating for paint or other organic materials. Chemical dip met hods are em ployed to create protective oxide films on iron, steel, stainless steel, alumin um, copper and some of their alloys. Such films are usually very thin and are frequently colored. Electrolytic coatings may be made, as in the case of a nodizing treat ments for alumin um which produce a relatively thick, abrasion resistant coating.

Vitreo us coatings alt hough brittle, possess surface h ard ness and complete inert ness to many corrosive environments. Enameled or glass lined vessels and ot her equip ment are available in a variety of s h apes and sizes. These en a mels a re made from fu sed silica tes of various compositions, containing colloidal suspensions of coloring materials. For metallic sheets, the enamel is applied as slurry. Subsequent heating conditions are dependent on enamel composition and intended service.

Organic Coatings:

These represent a large variety of materials and are the most widely used methods of protecting metals against corrosion. More than a thou sand different synthetic resins, as well as a wide variety of pigments, modifying oils and solvents are used in coating for mulation s. These coatings protect metals by interposing a continuous, adherent, inert film between the metal and its environmen t. They also markedly change the appearance of the metal. These coatings can be divided into three classes. Pain t is a dispersion of pigments in a vehicle which consists of drying oils modified with a solven t or thinner to aid in the application. Enamel is a dispersion of pigments in varnish or resin vehicle which polymerizes either by oxidation a troom tem perat u re or by application of heat. Lacquer is a pigmented natural or synthetic resin dissolved or suspen ded in solven ts. Powder coating is effectively carried out by applying a polymer by a spray or an

electrostatic spray followed by baking at high temperature. This results in a uniform continuous coating.

<u>Linings:</u>

Storage tanks, reaction vessels, pipes, ducting, etc. are covered with linings in order to (a) give the underlined structure protection against chemical attack, (b) prevent contamination of materialsbeing processed, and (c) minimize the effect of abrasion. The various materials commonly used for linings are rubber, lead, glass, plastic, acid proof bricks, etc. Fiber glass lining either Fiberglass Reinforced Epoxy (FRE) or Fiber Reinforced Polymers (FRP) are also widely used nowadays.

Case study of corrosion in a Spray Drying Tower used for producing blowndetergent towers:





Pictures of corrosion of spray drying tower

Analytical approach:

A. Observations - directly related to corrosion:

1. The NDT report shows that there are varying degrees of corrosion in the entire tower. However, the corrosion seems to be more prominen t and concentrated at the top support level of the tower where the feed to the spray dryer is likely to come in contact first with the shell; while not desirable, it cannot be com pletely avoided.

From the nature of the corrosion, as seen in the photographs, it appears to be the result of pitting and stress.

Alt hough, the full composition of the feed to the dryer is not known, it has been mentioned by the manufacturer that the feed contains salt as one of the constituents.

Keeping bot h t hese observation s in min d, it is highly possible t h a t one of the main reasons for corrosion is chloride stress.

2. The tower is constructed out of carbon steel SA515 / 516 Grade 60/70 and is not lined.

While lining or cladding is necessary to preven t expos u re of t he carbon steel and consequent deterioration, it must be pointed out that SS304 is not the right material to with stand the operating condition s. There are ot her grades of stainless steel such as SS316 or D u plex 2205 with higher content of nickel, chromium and molybden um which are better suited from the corrosion point of view.

Moreover, plug welding of the SS sheets to the parent metal locks in further stresses which contributes to chloride stress corrosion, nor mally seen as fine cracks. Further, technology has progressed with respect to techniques of linings. If cost is not the primary consideration, then "CLAD STEEL PLATE" produced by superior met hods of bonding can be used. However, for selection of the material of cladding, the composition of the feed must be known in far greater detail - if not the exact composition - at least the pH value and the salt content.



3. It is not yet determined whet her the corrosion is from inside to outside or outside to inside because in spection of the inside of t he tower is not possible unless it is shut down and also insulation on outside surface will need to be removed for inspection of the exter nal surface of the shell.

Further, it has been mentioned that the insulation of the tower is rock wool which contain s chemicals that can contribute to corrosion and is also hydrop hilic in nature.

While glass wool is uns uitable for the cylin drical part of the tower beca u se of heat, there are more appropriate option s s u ch as silica based aerogels and composite pyrogels, etc.

Therefore, it must be ascertained whether the corrosion is from inside to outside or outside to inside or a combination of both to understand whether corrosion is purely stress related or a com bin ation of both chloride stress att ack and reaction of in sulation material.

B. Other Observations – not directly related to corrosion, but important in the overall considerations:

1. The tower is supported at two floor levels. Due to the increase in the num ber of supports at multiple levels, there will be zones of stress concentration, particularly, the locked in residual s tresses at the welded connection s and reversal stresses due to restrain t sto expansion and contraction of the shell. These factors enhance the vulnerability to chloride stress corrosion.

Ideally the tower must be supported directly on columns with footings. Such supporting arrangement can also be designed by optimizing the load transfer path and foul checking with respect to the grade beams and foundations of the existing structure.

2 . It has been reported that the external surface of all the tower is pain ted "silver" (presumably referring to the "color" but it is assumed that the paint is aluminum based).
The exterior of the tower that is the parent metal side must be protected with suitable heat resistant coatings such as silicone base paints, multi-polymeric high build primer, etc. before insulating it.

This brief note must be considered as a preliminary attempt to identify the possible reasons for corrosion and suggested remedies.

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TRANSITIONING TO HIGH STRENGTH STEEL FOR STRUCTURAL APPLICATIONS

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INTRODUCTION

Application of high strength steel in structures aids in achieving higher economy, whichhowever is accompanied by decrease in ductility and section size. This leads to increase in stress rangeand possibility of pre-mature failure of section due to local and/or global instabilities in the members. Variation in the nominal to expected yield and ultimate strength can also become critical in structures where strong colum n-weak beamphilosop hy has to be achieved for better performance.

Steel structural system s like moment resisting frames (MRF), concentrically braced frames (CBF) and eccentrically braced frames (EBF) included in steel design code IS 800:2007, are popularly used in industrial as well as commercial buildings. These systems depend upon deformation-controlled elements like beams in MRF, braces in CBF and link elements in EBF to dissipate energy during an extreme loading condition like eart hquake, so as to act like a "fuse" and safegu ard the critical gravity load carrying members like beam and column (force-controlled elements). This hierarchy of member and connection's strength and ductility, which con sequently affects the overall performance of the structure can only be achieved if an engineer understands the steel material characteristics in the elastic and inelastic stages as well as has design procedures accommodating the higher strength of steel. IS800: 2007 guidelines allow use of E250B grade in MRF and CBF and additionally the inclusion of 27 J energy criteria requirement can push this to E350 grade

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as per IS 2062:2011. In ter n a tion al codes allow higher grade steels for force con trolled elements, which can lower the cost of the structure. However, as men tioned above the u se of higher strengths teel has to be done with caution, especially in the case of built-up sections, where inform a tion about the perform ance of high strengths teel plates at material level, component level as well at an assembly/frame level are not available in plenty.

As a first step towardstransitioning into utilizing higher strength steel and u sing adva need design met hodology like perfor m a nee-based design to economically build structures that achieve specific targeted performance under extreme loading condition like eart hq u ake, m a terial ch a racterization of three grades of Indian steel E250, E350 and E450 has been taken up.

MATERIAL CHARACTERIZATION STUDY

The ongoing study currently focuses on base metal characterization of different grades of steel. This is being done through exhaustive monotonic as well cyclic testing of coupon test specimen s extracted from the base metal. The specimen includes convention al coupon specimen as per ASTM E8 as well as various notched specimens [Fig. 1(a)] fabricated to develop varied stress triaxiality, lode a ngle and equivalent plastic strain, which can then be directly related to different structural systems as well as connection s at the mem ber level [Fig. 1(b)].

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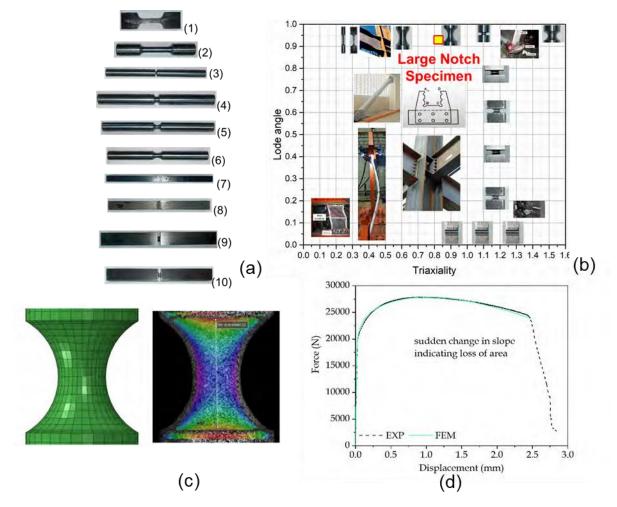


Fig 1: Material characterization study overview with results presented for one large notch specimen

Digital im age correlation (DIC) system shave been u sed to acquire complete spectrum of data from the elastic stage, through plastic deformation phase to the fin al failu re of the coupon specimen[Fig. 1(c)]. Num erical validation of the experimental tests has been conducted through finite element simulation to obtain para meters for the material constitutive model [Table 1] as well as the fracture locus. The validation of one of the large notch coupon specimens[(Fig. 1(d)] as well as its fracture locusis highlighted in [Fig. 1(b)]. This data will helpt he engineering community to move to economical and performance enhanced s tructural systems while appreciating and accommodating the changes required to incorporate high strength steel into design.

Specimen	f _y (MPa)	Q∞ (MPa)	b	C ₁ (MPa)	G1	C ₂ (MPa)	G ₂
LN (E250)	340	60	100	1500	7	200	4
LN (E350)	430	125	100	1500	7	200	4
LN (E450)	535	87.5	100	1500	8	200	4

 Table 1: Combined hardening parameters for differentsteel grades

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